



HIL TESTING OF AUTOMATIC VOLTAGE SETPOINT OPTIMIZER FOR A CLUSTER OF WIND FARMS

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2023 North American
RTDS
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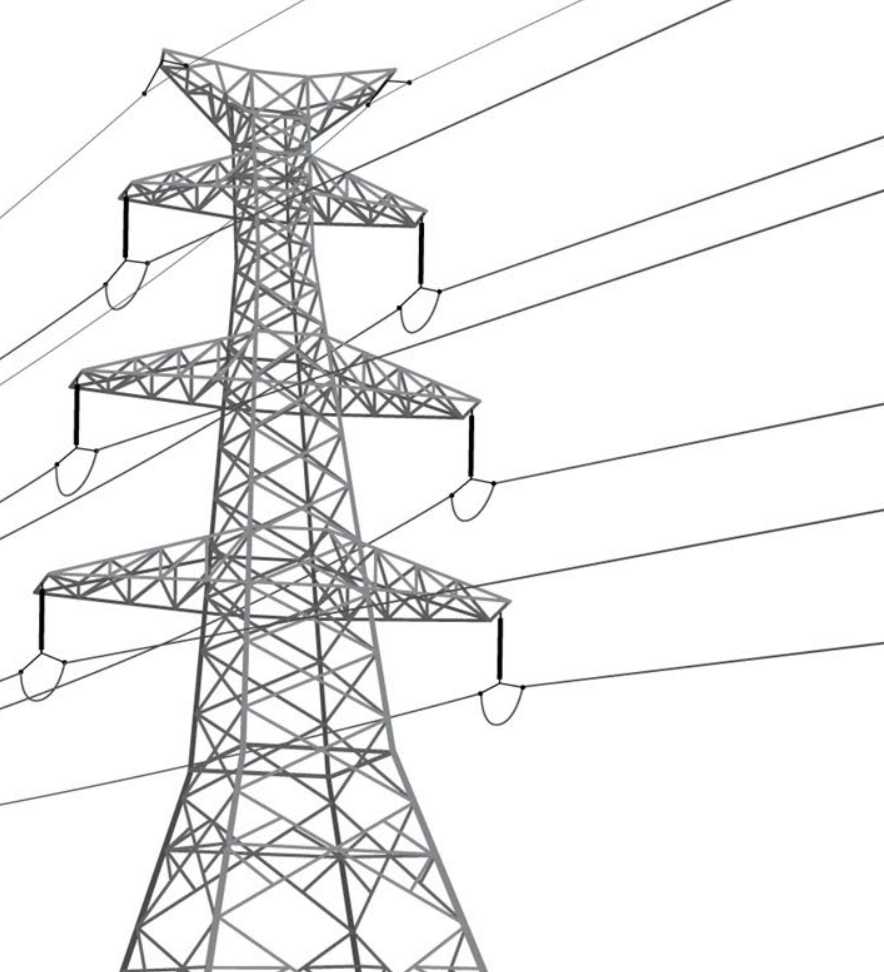
Introduction - TGS

- We are a power systems consulting company based in Winnipeg, Canada.
- 20 years in the industry
- Experts in:
 - HVDC/FACTS
 - Power System Analysis
 - Renewable Energy integration studies
 - PSCAD/RSCAD – model development
 - RTDS HIL Testing



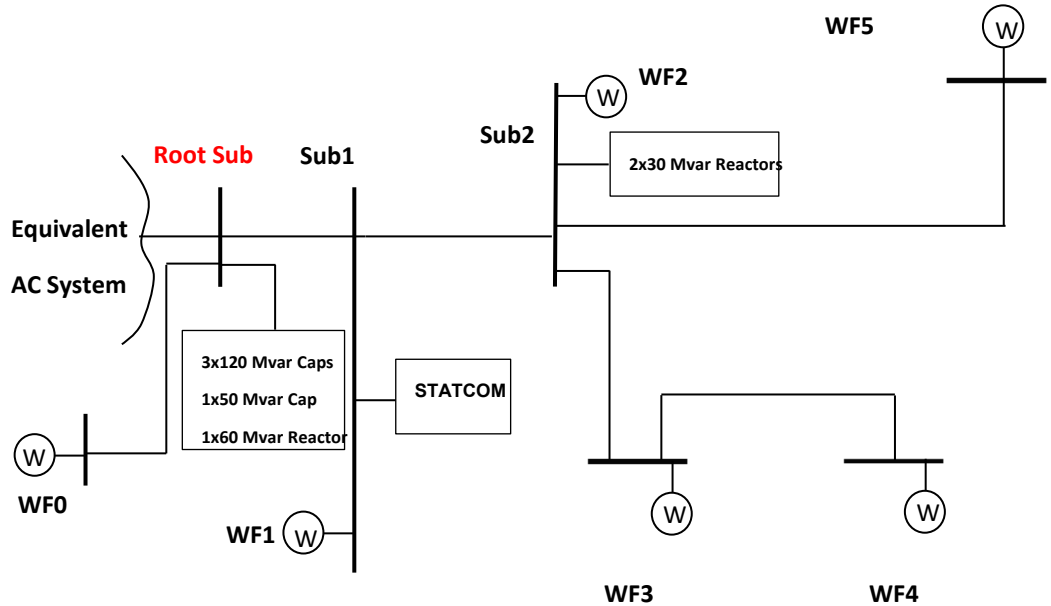


Overview



Overview

- Cluster of windfarms connected to a 345kV radial backbone
- Wind farms - multiple owners, multiple manufacturers, multiple PPCs and EMSs
- Reactive power management criterion is based on tight voltage regulation at the Root Substation at 1.02 pu
- Client - Developer of the firmware solution
- Client of the client - Transmission owner - a utility company in the USA.





Client-Proposed Solution

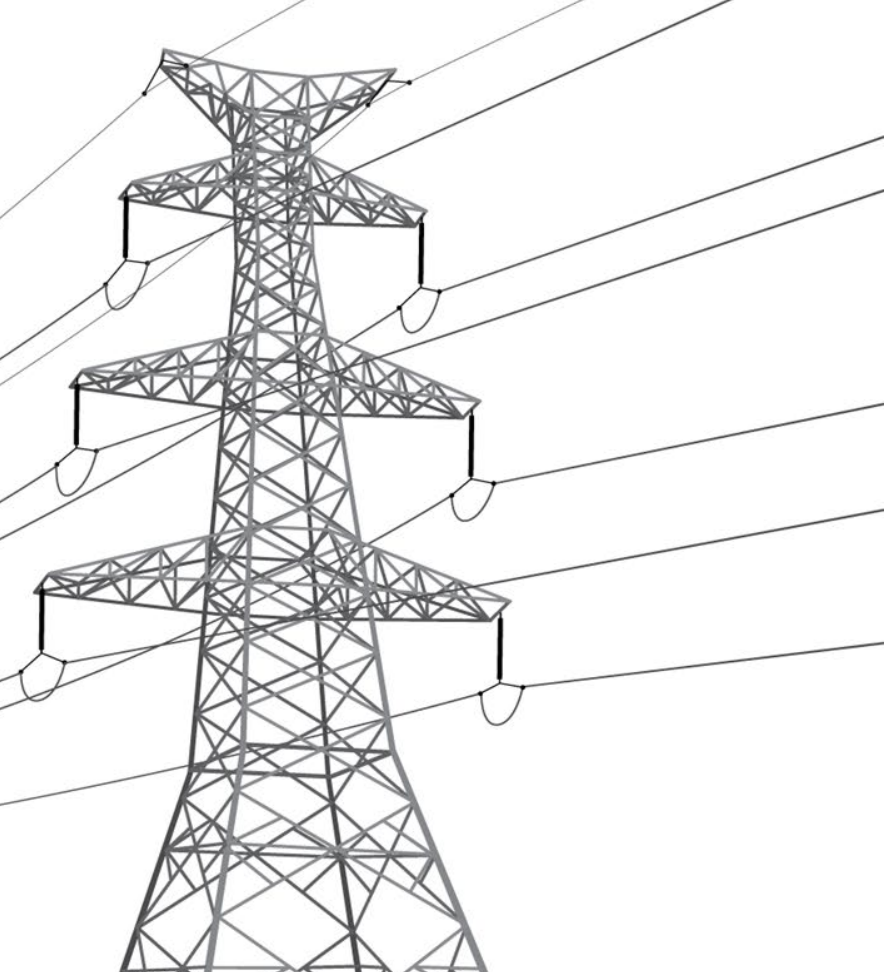
- Dynamically change the voltage setpoints of all windfarms and the STATCOM, based on their available reactive power capability to achieve 1.02pu at the Root Substation.

HIL Test Requirement

- Prove to the transmission system operator that the proposed solution work through a witnessed FAT



RTDS Test Setup



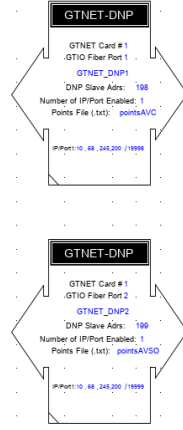
Hardware Used

- 3 RTDS Racks (PB5) – AC system Model
- GTNETx2 Card – Communication Between RTDS and RTACS
- 2x SEL-3555 RTACs – AVSO primary and secondary controllers
- 2x SEL-3530 RTACs – Root substation AVC and Substation-2 AVC
- 1x SEL-3505 RTACs – EMS emulator
- HMI Interface



GTNET DNP Configuration

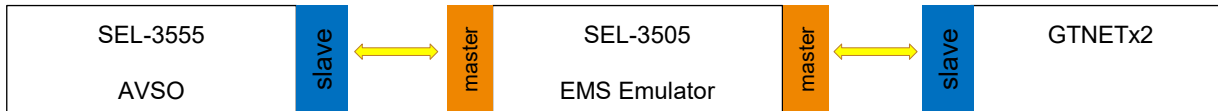
- GTNET card can only act as a DNP slave
- AVSO/AVC RTACs act as:
 - **Slave** to measurement RTUs
 - **Master** to WPP PPCs
- The SEL-3505 acted as a master-master intermediary so that all for RTU measurement communication RTDS appear as master to AVSO/AVC and master to GTNET card as well

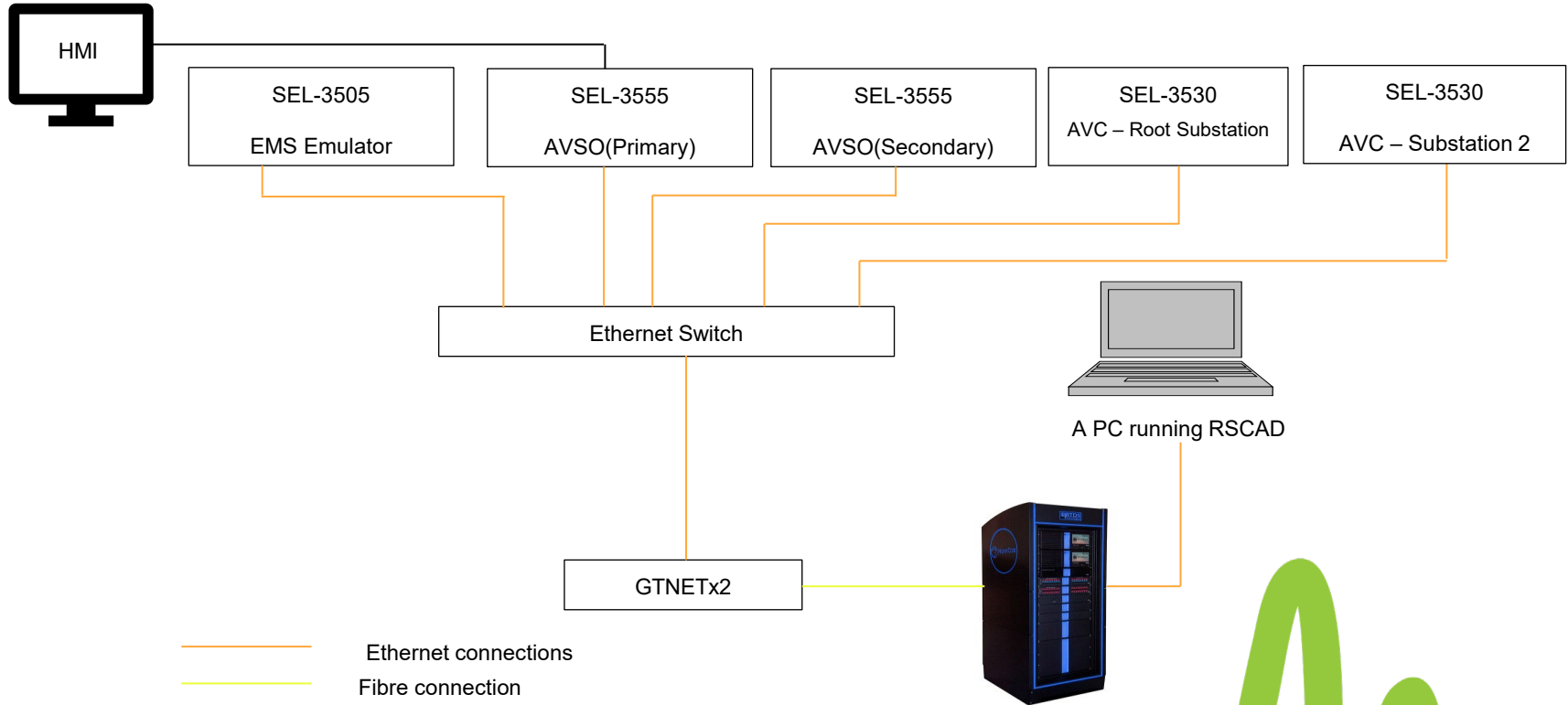


RSCAD DNP Component

#	BI	Binary Input Object	1,2 in DNP Specification	(Outputs from RTDS)
1				
2				
3	BI: 0	WPP6_BKR_STATUS_E37211	WPP6_BKR_STATUS	0
4	BI: 2	WPP6_BKR_STATUS_E37212	WPP6_BKR_STATUS	1
5	BI: 4	WPP6_BKR_STATUS_7215	WPP6_BKR_STATUS	2
6	BI: 6	WPP6_BKR_STATUS_1150	WPP6_BKR_STATUS	3
7	BI: 7	WPP6_BKR_STATUS_1250	WPP6_BKR_STATUS	4
8	BI: 8	WPP6_SW_STATUS_1151	WPP6_BKR_STATUS	5
9	BI: 12	WPP6_SW_STATUS_1152	WPP6_BKR_STATUS	6
10	BI: 16	WPP6_SW_STATUS_1153	WPP6_BKR_STATUS	7
11	BI: 20	WPP6_SW_STATUS_1251	WPP6_BKR_STATUS	8
12	BI: 24	WPP6_SW_STATUS_1252	WPP6_BKR_STATUS	9
13	BI: 28	WPP6_SW_STATUS_1253	WPP6_BKR_STATUS	10
14	BI: 32	WPP6_MOD_STATUS_7215N	WPP6_BKR_STATUS	11
15	BI: 33	WPP6_MOD_STATUS_7215S	WPP6_BKR_STATUS	12
16	BI: 34	WPP6_MOD_STATUS_7199	WPP6_BKR_STATUS	13
17				
18	BI: 1	WPP6_BKR_LOCKOUT_E37211	WPP6_B1STATUS2	0
19	BI: 3	WPP6_BKR_LOCKOUT_E37212	WPP6_B1STATUS2	1
20	BI: 5	WPP6_BKR_LOCKOUT_7215	WPP6_B1STATUS2	2
21	BI: 9	WPP6_SW_LOCKOUT_1151	WPP6_B1STATUS2	3
22	BI: 10	WPP6_REMOTE_STATUS_1151	WPP6_B1STATUS2	4
23	BI: 11	WPP6_UNBALANCE_1151	WPP6_B1STATUS2	5
24	BI: 13	WPP6_SW_LOCKOUT_1152	WPP6_B1STATUS2	6
25	BI: 14	WPP6_REMOTE_STATUS_1152	WPP6_B1STATUS2	7
26	BI: 15	WPP6_UNBALANCE_1152	WPP6_B1STATUS2	8
27	BI: 17	WPP6_SW_LOCKOUT_1153	WPP6_B1STATUS2	9
28	BI: 18	WPP6_REMOTE_STATUS_1153	WPP6_B1STATUS2	10
29	BI: 19	WPP6_UNBALANCE_1153	WPP6_B1STATUS2	11
30	BI: 21	WPP6_SW_LOCKOUT_1251	WPP6_B1STATUS2	12
31	BI: 22	WPP6_REMOTE_STATUS_1251	WPP6_B1STATUS2	13
32	BI: 23	WPP6_UNBALANCE_1251	WPP6_B1STATUS2	14
33	BI: 25	WPP6_SW_LOCKOUT_1252	WPP6_B1STATUS2	15
34	BI: 26	WPP6_REMOTE_STATUS_1252	WPP6_B1STATUS2	16
35	BI: 27	WPP6_UNBALANCE_1252	WPP6_B1STATUS2	17
36	BI: 29	WPP6_SW_LOCKOUT_1253	WPP6_B1STATUS2	18
37	BI: 30	WPP6_REMOTE_STATUS_1253	WPP6_B1STATUS2	19
38	BI: 31	WPP6_UNBALANCE_1253	WPP6_B1STATUS2	20
39	BI: 35	WPP6_TR1_LTC_OFF_TAP_POSITION	WPP6_B1STATUS2	21
40	BI: 36	WPP6_TR1_LTC_AUTO_MANUAL_STATUS	WPP6_B1STATUS2	22
41	BI: 37	WPP6_TR1_LTC_REMOTE_LOCAL_STATUS	WPP6_B1STATUS2	23
42	BI: 38	WPP6_TR2_LTC_OFF_TAP_POSITION	WPP6_B1STATUS2	24
43	BI: 39	WPP6_TR2_LTC_AUTO_MANUAL_STATUS	WPP6_B1STATUS2	25
44	BI: 40	WPP6_TR2_LTC_REMOTE_LOCAL_STATUS	WPP6_B1STATUS2	26

Points list for the AVSO RTAC





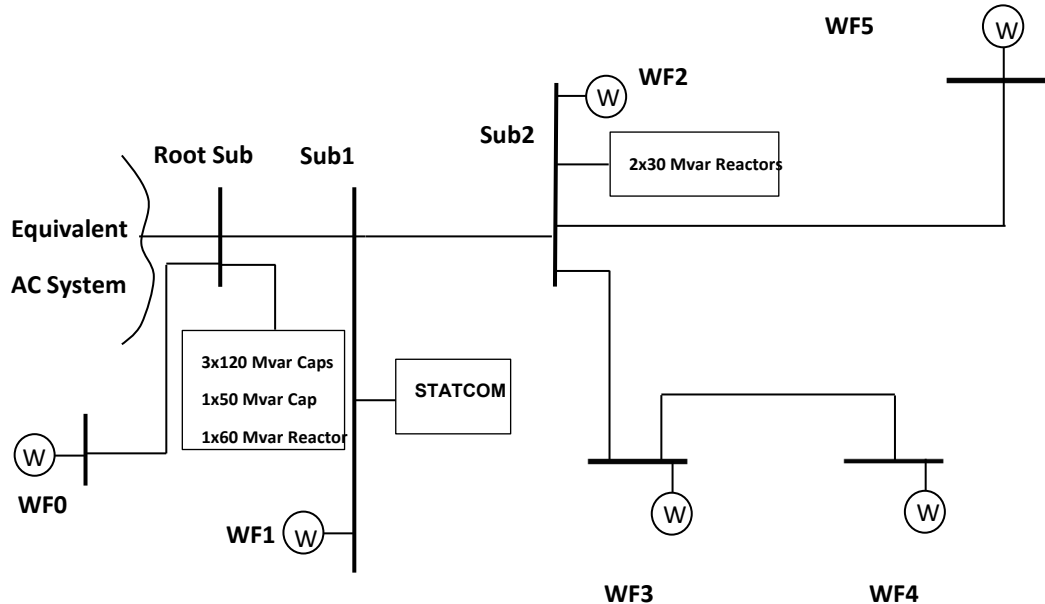


RSCAD Model



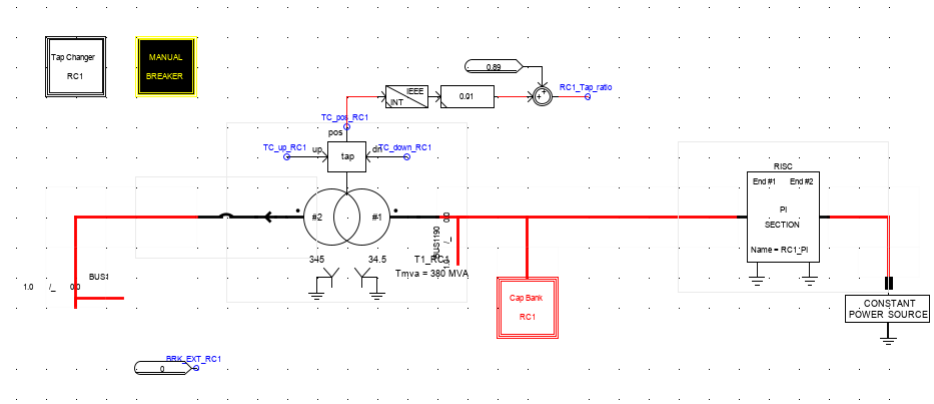
AC Network Model

- Only PCC voltage regulation is modelled
- Aggregated model of WF0 is also included
 - Controls Root Substation voltage with line droop compensation
 - Voltage regulator response time = 40 s



Wind Farm Models

- Each wind farm in the Gen-tie has been modeled as a lumped controlled PQ source (Benchmarked with PSCAD response)
- PQ capability modelled as per Vestas 2.2MW and 2.0MW turbine specification
- For WF5: Assumed capable to maintain +/-0.95 pf.
- Collector system and pad mount transformer impedances are represented by a PI section model.
- MV Capacitor and Reactor banks and their switching logic has been modeled.
- Grid interface transformers have been modeled with the tap changer logic.



- MV shunt switching of the Gen-tie facilities are modelled

WF1

- Switch in capacitors at 60% of Q at PCC
- Switch off capacitors at 20% of Q at PCC
- Switch 2 reactors if P less than 60 MW for 3 minutes
- Switch remaining reactors if P less than 60 MW for an additional 3 minutes
- When P is above 60 MW for 3 minutes switch off one reactor every 3 minutes

WF2

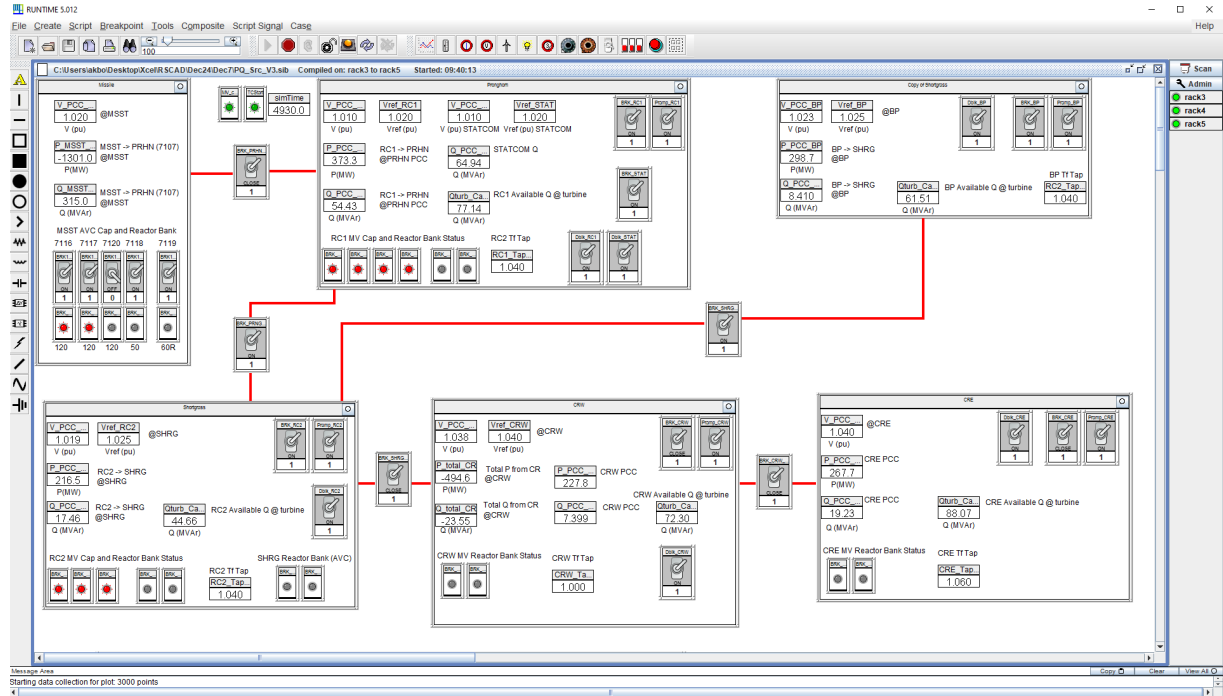
- Switch in capacitors at 60% of Q at PCC
- Switch off capacitors at 20% of Q at PCC
- Switch 1 reactor if P less than 60 MW for 3 minutes
- Switch remaining reactors if P less than 60 MW for an additional 3 minutes
- When P is above 60 MW for 3 minutes switch off one reactor every 3 minutes

WF3 and WF4

- Switch 2 reactors if P less than 10% for 3 minutes
- Switch remaining reactors if P less than 10% for an additional 3 minutes
- When P is above 10% for 3 minutes switch off one reactor every 3 minutes

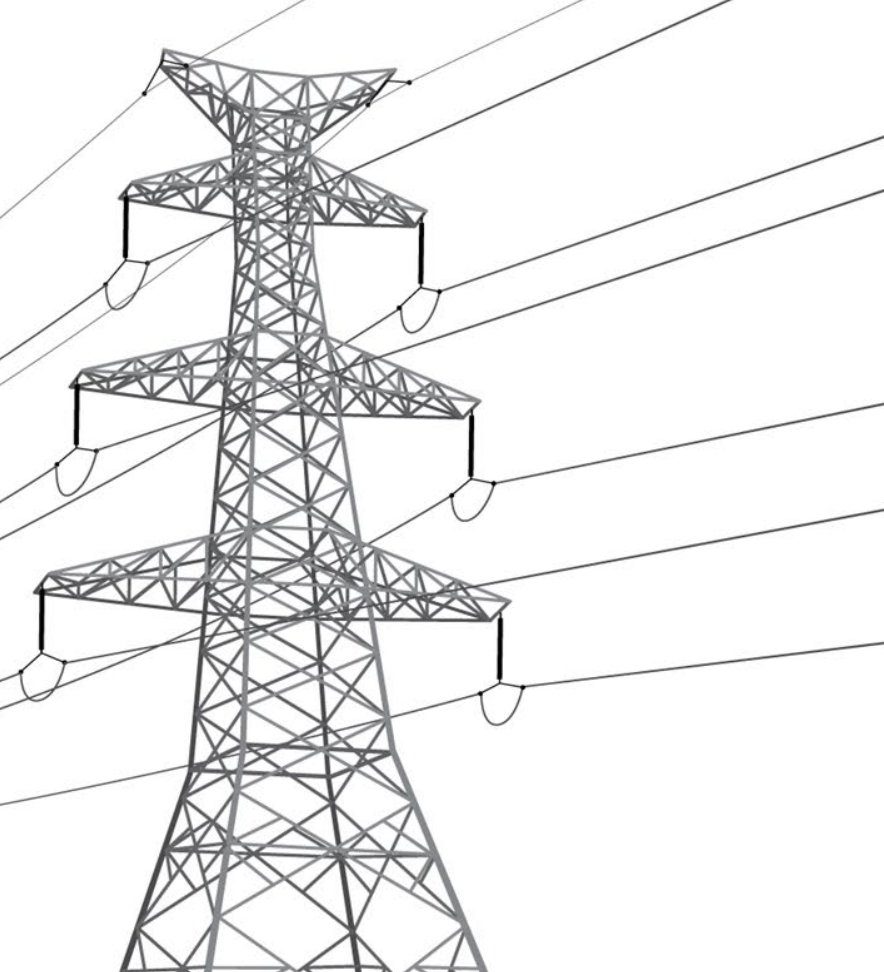
RSCAD Runtime

- RSCAD Runtime captures the plots required for offline analysis.
- The runtime has been setup to view voltages, power readings and capacitor/reactor statuses in real time.
- Necessary interventions can be done using the switches, in real time.





Tests

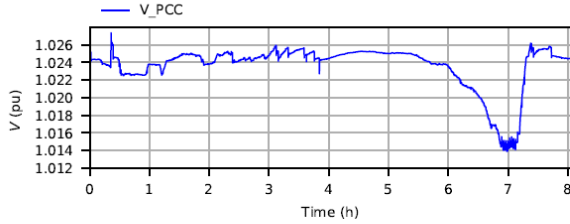


- Power ramp tests
- Root substation voltage step changes
- Facility trip tests
- Line trip tests
- Loss of signal tests
- Continuous operation
- Gen-tie energization
- AVSO primary-secondary change over

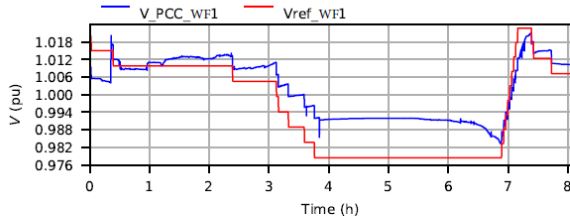
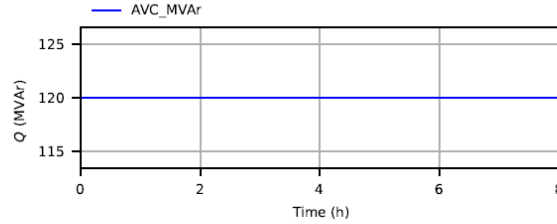
Sample Results

CO

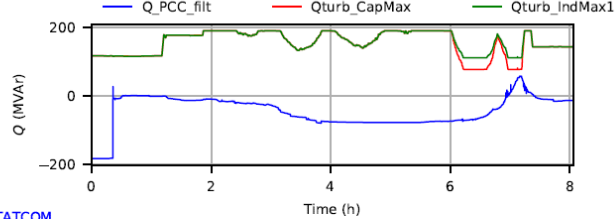
Continuous Operation Test (8 hours)



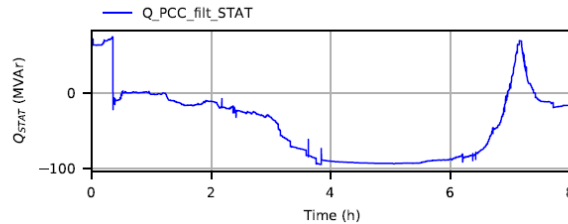
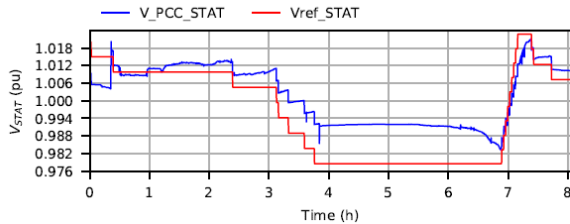
Root Sub



WF1

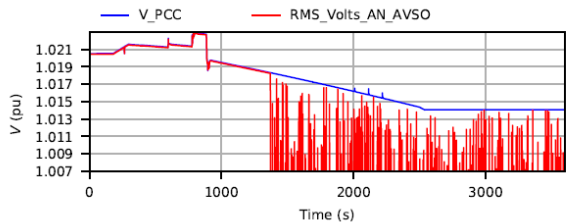


STATCOM

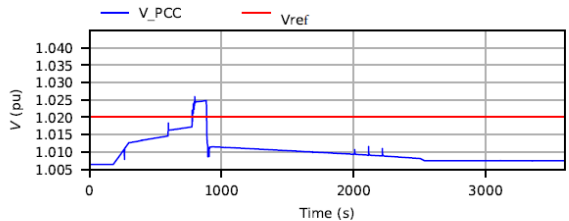
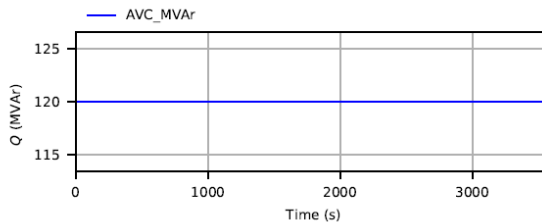


Sample Results

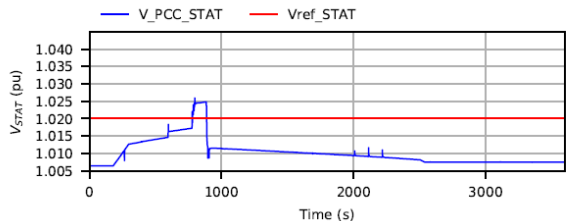
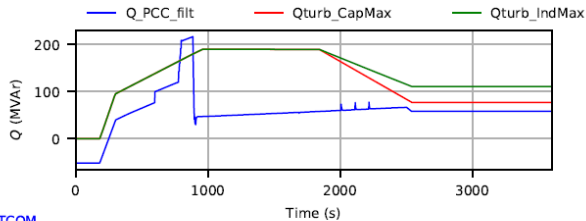
LS4 Malfunction of Root_M650_7170 Meter during WF1 ramp up



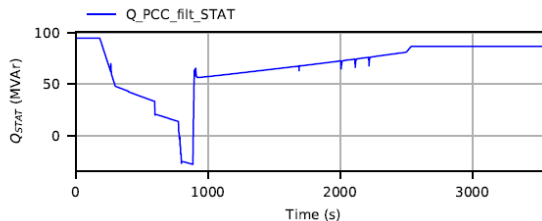
Root Sub



WF1



STATCOM

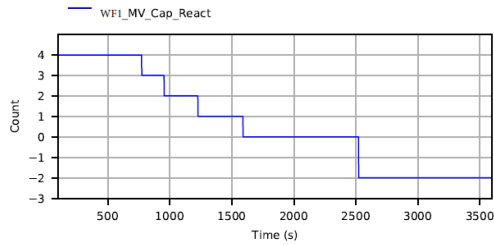


Sample Results

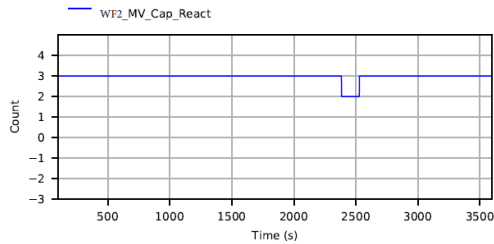
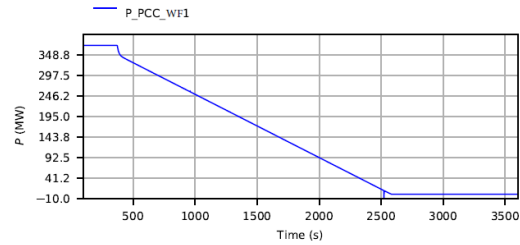
Power ramp down test (1/2)

PR1

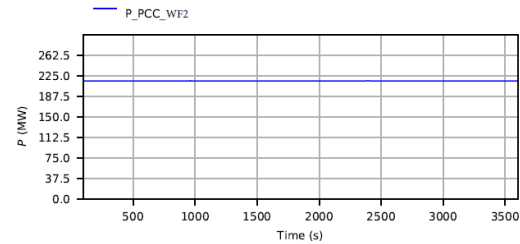
WF1 ramp down 100%-0% @2.5%/min



WF1



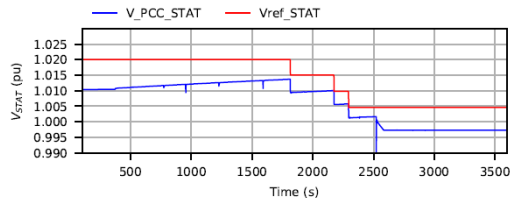
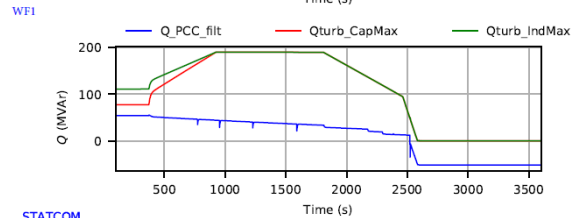
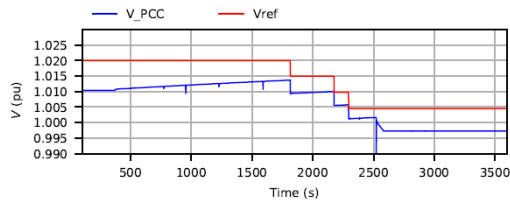
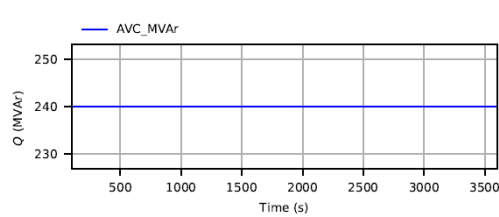
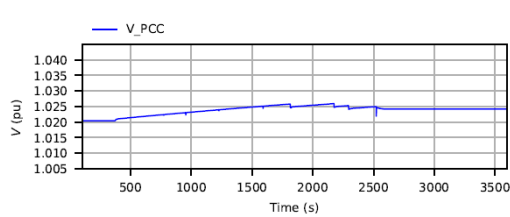
WF2



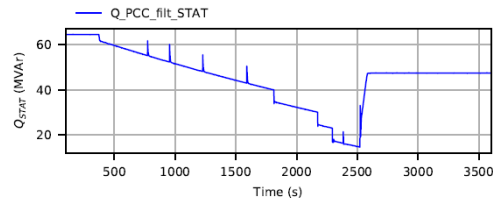
Power ramp down test (2/2)

PR1

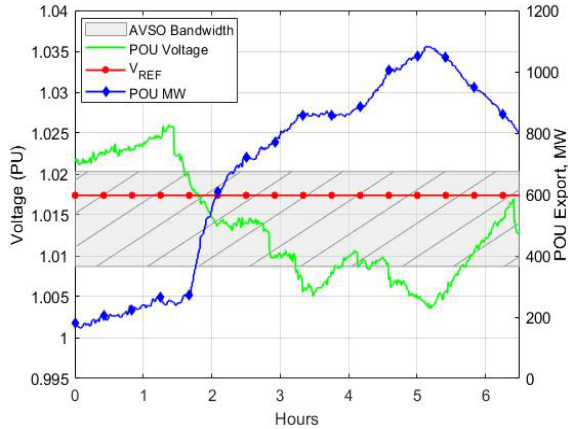
WF1 ramp down 100%-0% @2.5%/min



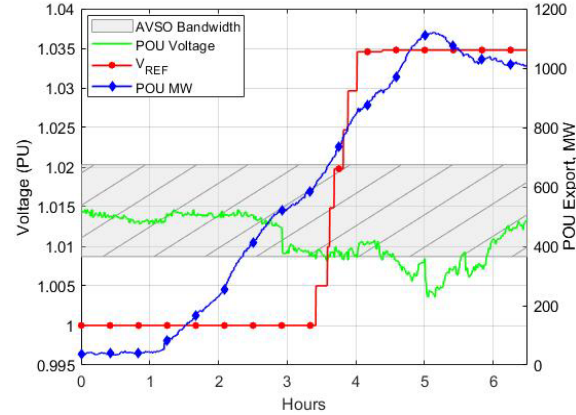
STATCOM



Field Measurements



System response to wind-ramp event
pre-AVSO implementation



System response to wind-ramp event
post-AVSO implementation



Challenges

- Pandemic! – Entire project, including FAT, was carried out remotely
- Remote debugging
- Time constraints – Wind Farms were already in operation. The studies portion of the AVSO development was embedded with HIL testing, saving precious time



Conclusions

- Inverter-based resource integration demands for high-level automatic system control to assist with operator task offload and voltage coordination.
- RTDS and field testing provided operators and engineers the confidence that the AVSO would handle unique operating scenarios
- FATs and HIL testing used to require travel, but this FAT was done entirely remotely, with a timely delivery
- RTDS is not only for studying fast transients. It was very useful in this slower voltage control testing
- RTDS studies for slower dynamics can be done without the full manufacturer models. Simple RSCAD models benchmarked with PSCAD models served the purpose.

Thank You