



IMPEDANCE-BASED STABILITY ANALYSIS OF A POWER HARDWARE IN-THE-LOOP FOR GRID-FOLLOWING INVERTER TESTING

FARGAH ASHRAFIDEHKORDI

KARLSRUHE INSTITUTE OF TECHNOLOGY

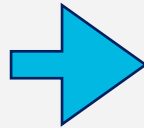


OUTLINE

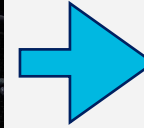
- ⇨ Why Power Hardware-in-the-Loop (PHIL)?
- ⇨ What are the challenges?
- ⇨ Impedance-based stability analysis
- ⇨ Simulation verification
- ⇨ Experimental results
- ⇨ Conclusion

WHY PHIL?

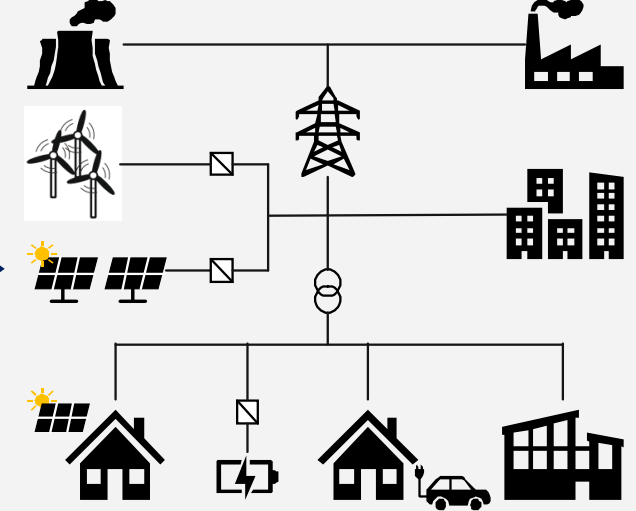
Power Hardware



PHIL



Power Grid



CHALLENGES OF PHIL



Ideal Scheme →

Digital real-time simulator (DRTS)



Hardware under test (HuT)

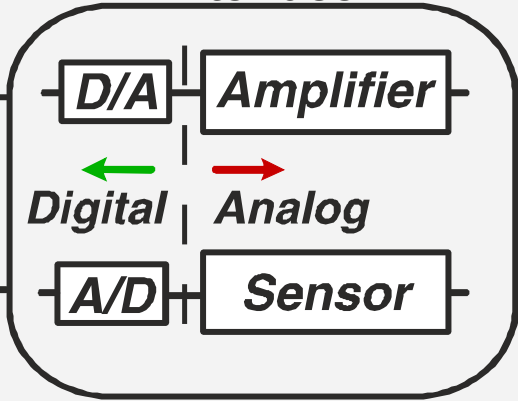


Existing Scheme →

DRTS



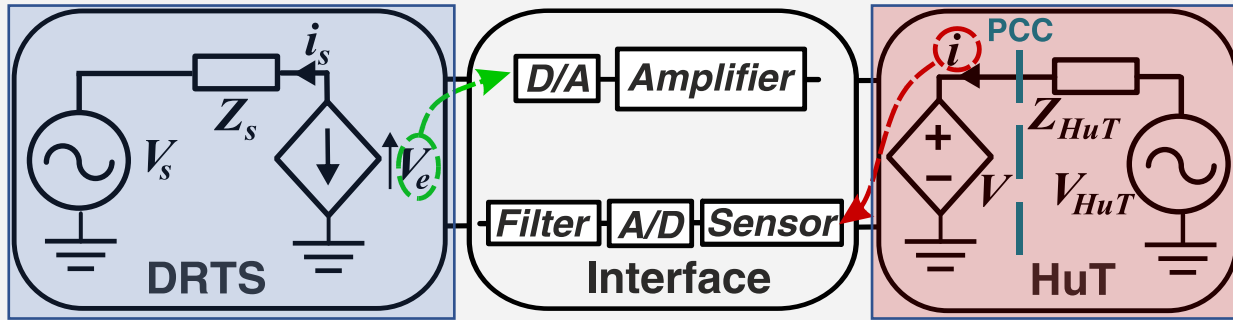
Interface



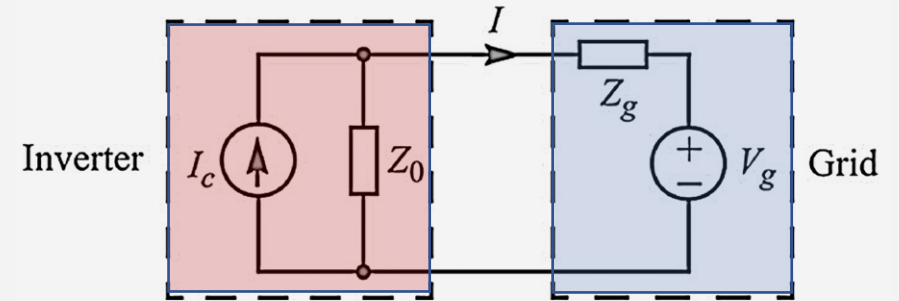
HuT



IMPEDANCE-BASED STABILITY ANALYSIS



Voltage-type Ideal Transformer Method (V-ITM)

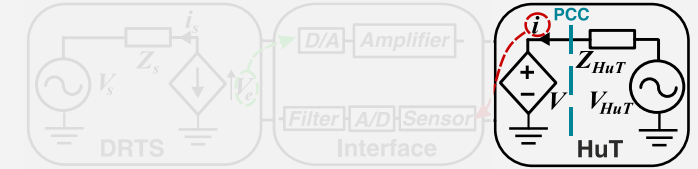
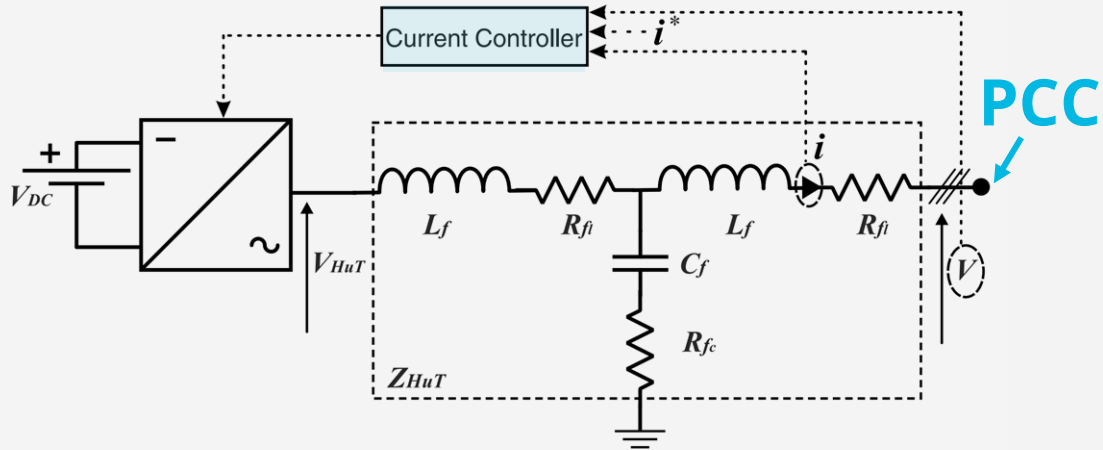


$$G_{OL} = ?$$

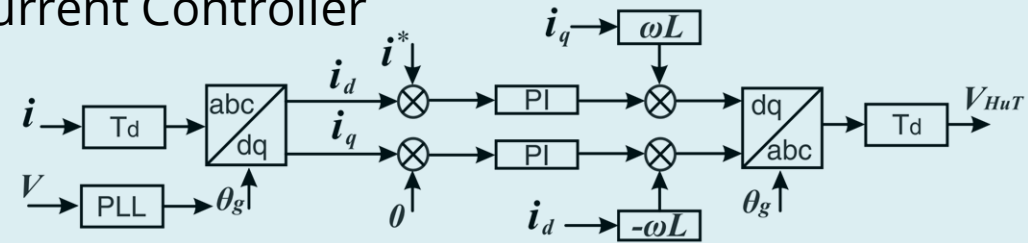
$$I(s) = \left[I_c(s) - \frac{V_g(s)}{Z_0(s)} \right] \frac{1}{1 + \underbrace{Z_g(s)/Z_0(s)}_{G_{OL}}}$$

[1] J. Sun, "Impedance-Based Stability Criterion for Grid-Connected Inverters," in IEEE Transactions on Power Electronics, vol. 26, no. 11, pp. 3075-3078, Nov. 2011, doi: 10.1109/TPEL.2011.2136439

IMPEDANCE MODEL OF THE GRID-FOLLOWING INVERTER



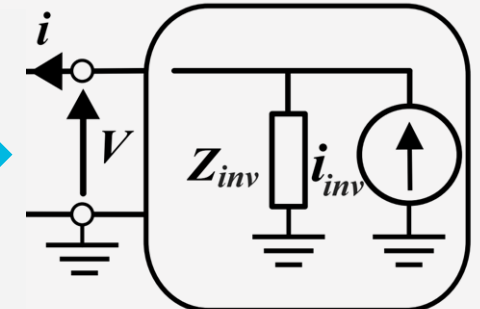
Current Controller



$$i = Y_{LCL, V_{HuT}}(s) \cdot \underline{V_{HuT}} + Y_{LCL, V}(s) \cdot V$$

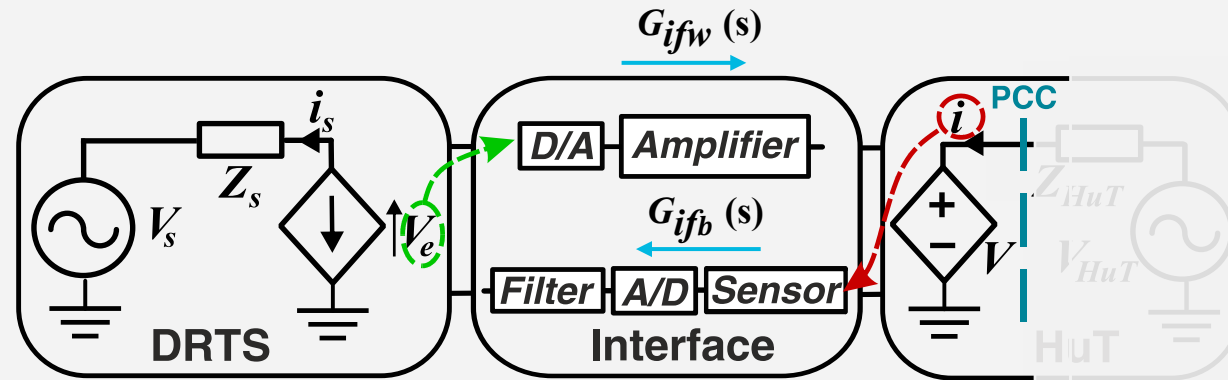
$$\underline{V_{HuT}} = (i^* - T_d(s) \cdot i) \cdot G_{PI}(s) \cdot T_d(s)$$

$$i = \underbrace{\frac{G_{PI}(s) \cdot T_d(s) \cdot Y_{LCL, V_{HuT}}(s)}{1 + G_{PI}(s) \cdot T_d(s)^2 \cdot Y_{LCL, V_{HuT}}(s)}}_{H_{inv}(s)} i^* - \underbrace{\frac{Y_{LCL, V}(s)}{1 + G_{PI}(s) \cdot T_d(s)^2 \cdot Y_{LCL, V_{HuT}}(s)}}_{Y_{inv}(s)} V$$



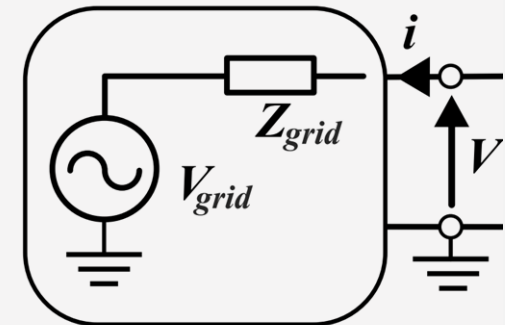
$$i_{inv} = H_{inv}(s) \cdot i^*$$

IMPEDANCE MODEL OF THE GRID



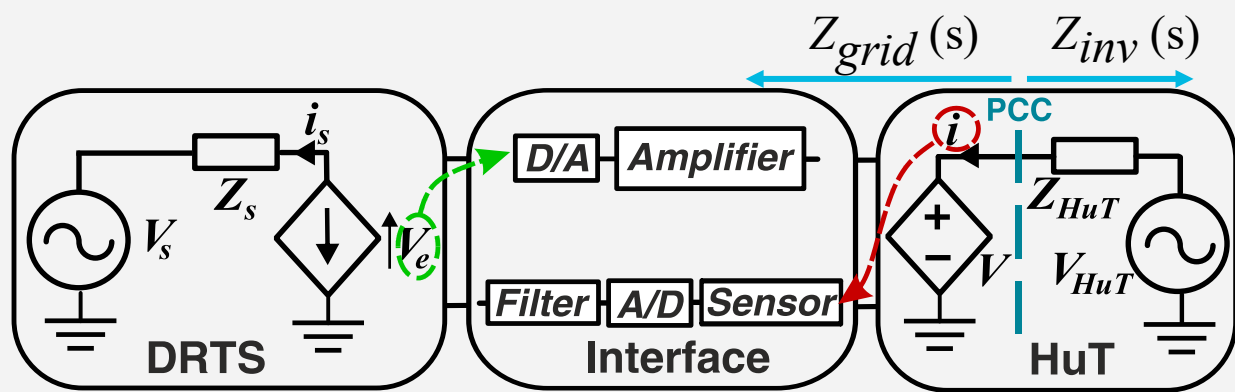
$$V = \overbrace{(V_s + G_{ifb}(s) \cdot Z_s(s) \cdot i)}^{V_e} \cdot G_{ifw}(s)$$

$$i = \underbrace{\frac{1}{G_{ifb}(s) \cdot Z_s(s)}}_{H_{grid}(s)} V_s - \underbrace{\frac{1}{G_{ifb}(s) \cdot Z_s(s) \cdot G_{ifw}(s)}}_{Y_{grid}(s)} V$$

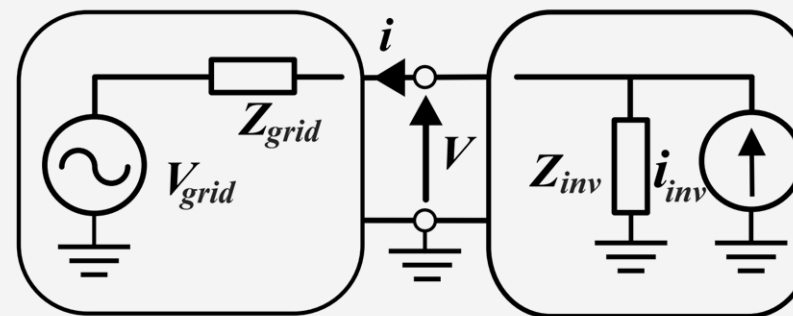


$$V_{grid} = H_{grid}(s) \cdot V_s$$

STABILITY CRITERION



Existing PHIL Model



Impedance Model



$$G_{OL} = \frac{Z_{grid}(s)}{Z_{inv}(s)}$$

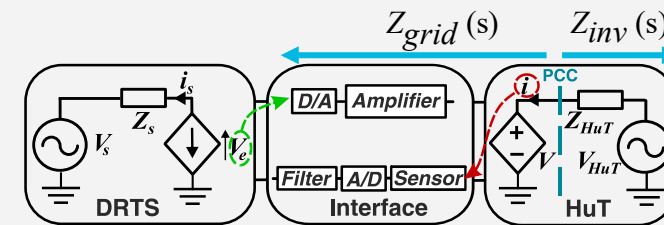


Nyquist Plot



Simulink Model

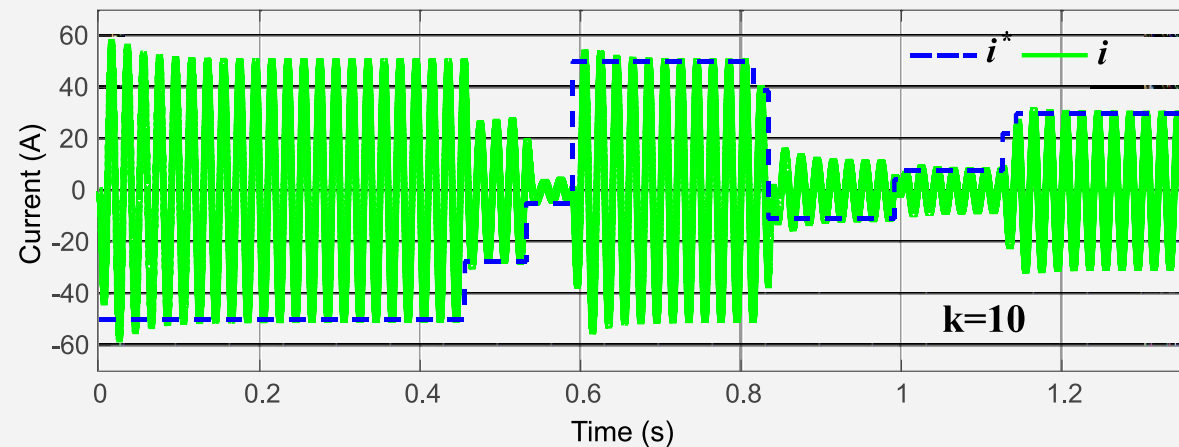
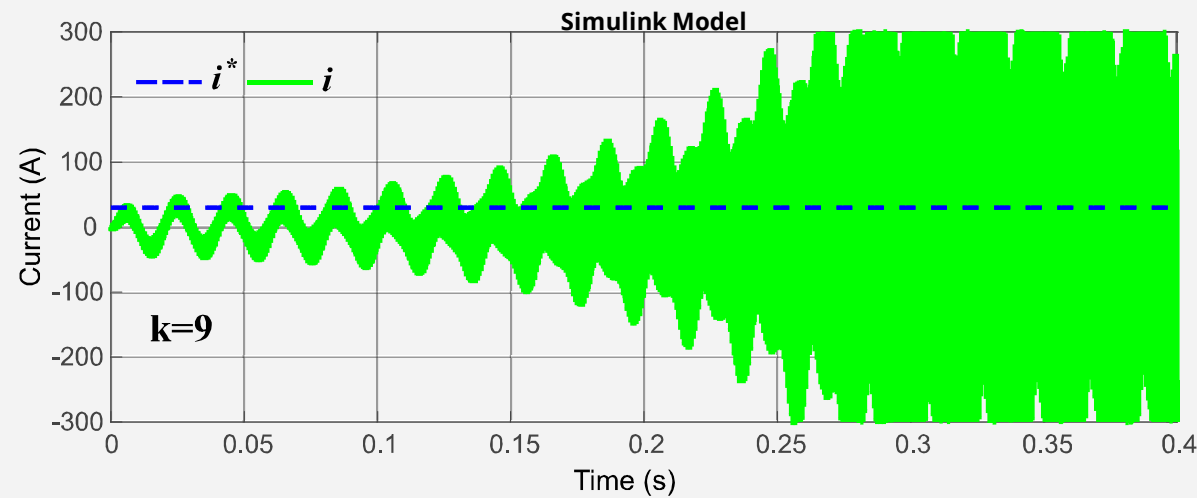
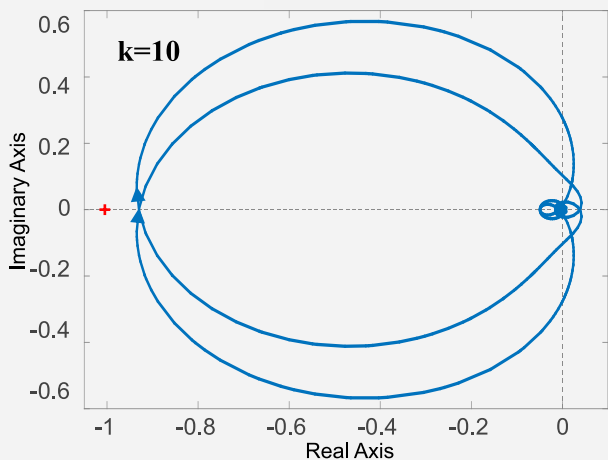
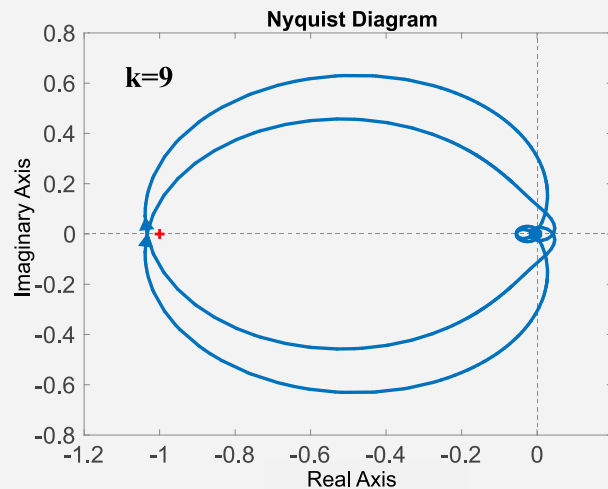
STABILITY VERIFICATION



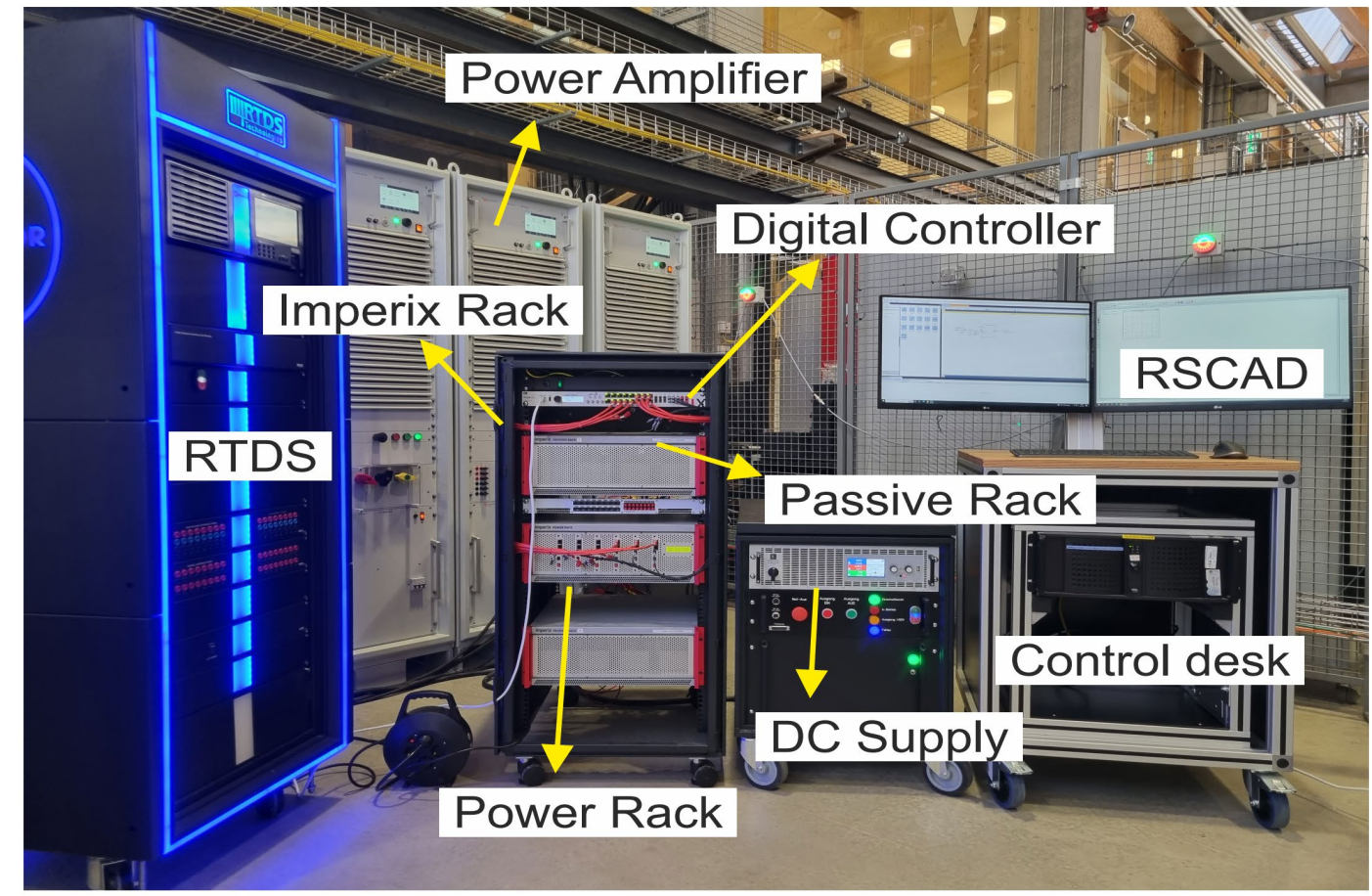
$$G_{OL} = \frac{Z_{grid}(s)}{Z_{inv}(s)}$$

Inductive part of Z_{HuT}

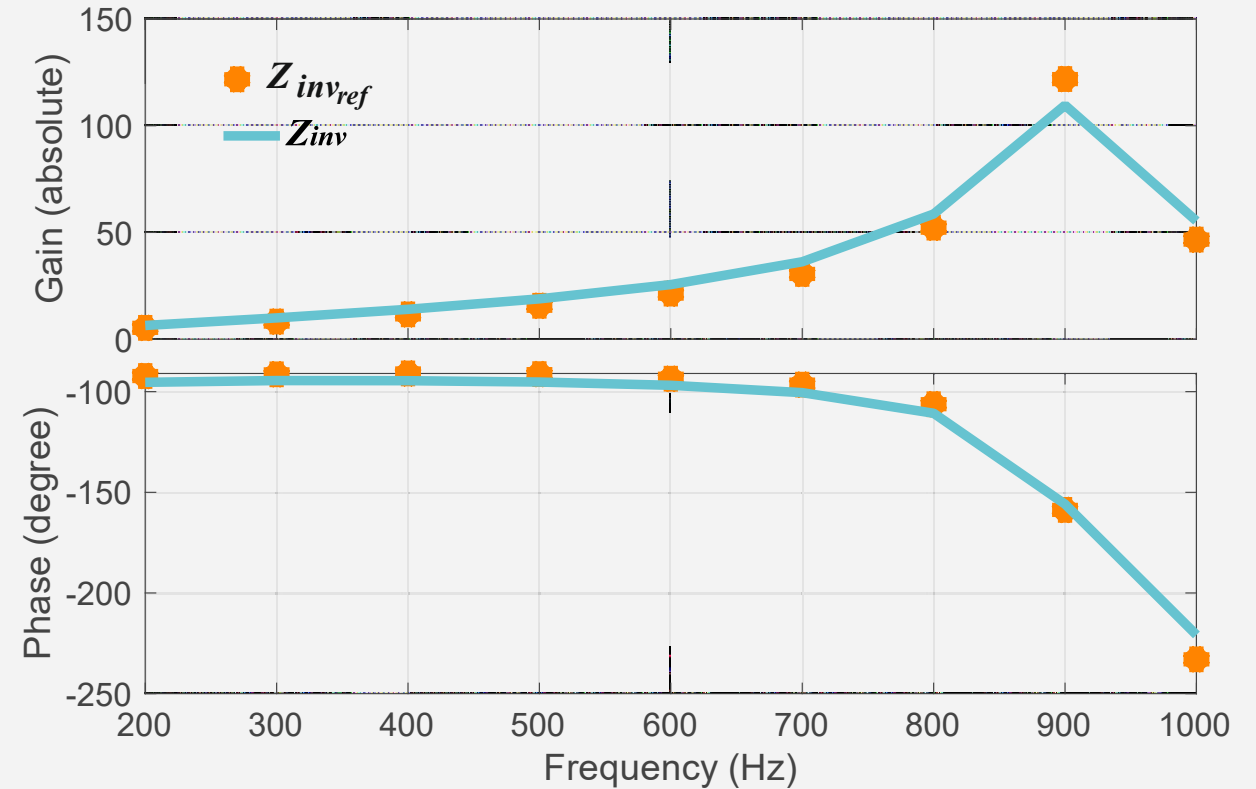
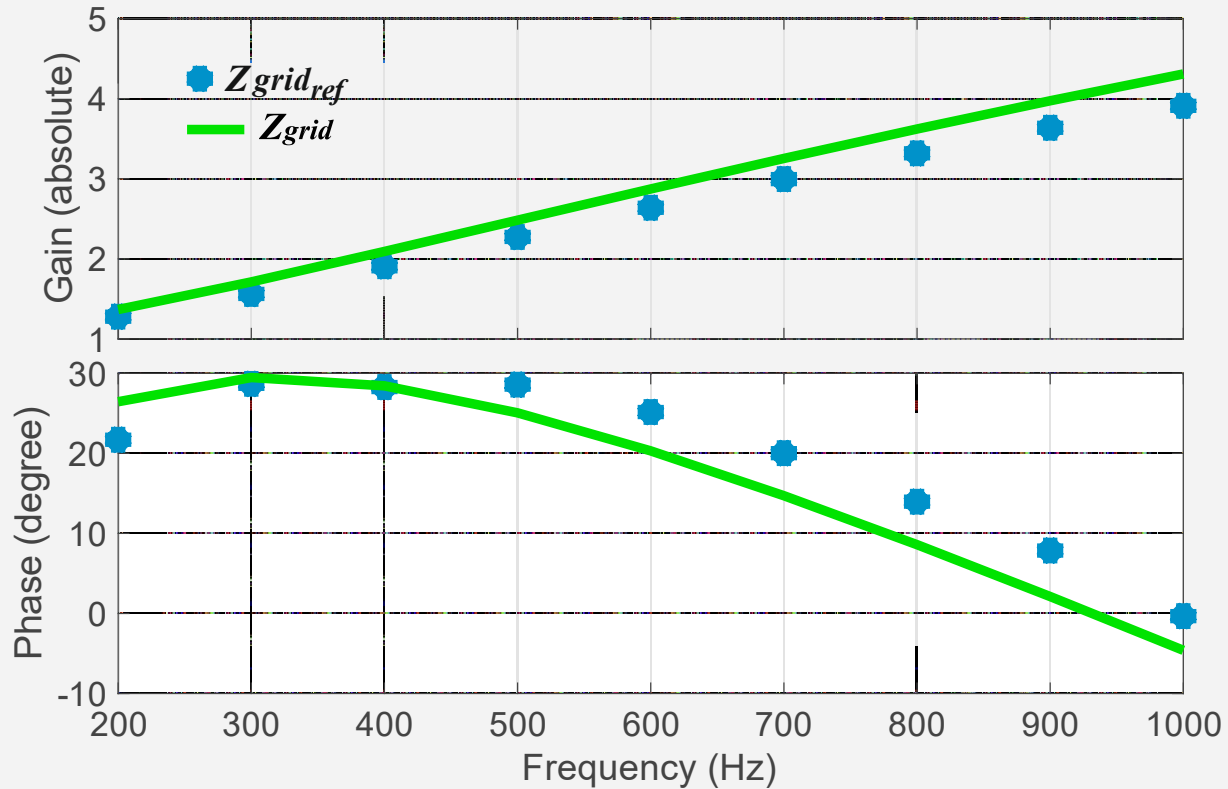
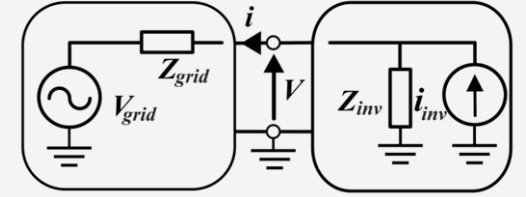
$$k = \frac{Z_L(s)}{Z_S(s)}$$



PHIL SETUP AT ENERGY LAB 2.0



IMPEDANCE VERIFICATION



CONCLUSION

- ⊖ Impedance-based stability, straightforward and accurate
- ⊖ Impedance information is necessary and sufficient
- ⊖ Proper approach to ensure stability unknown HuT

THANK YOU!

Any
Questions?

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