

Real-time Simulation of Transformer Differential Protection based on Clarke-Wavelet Transform

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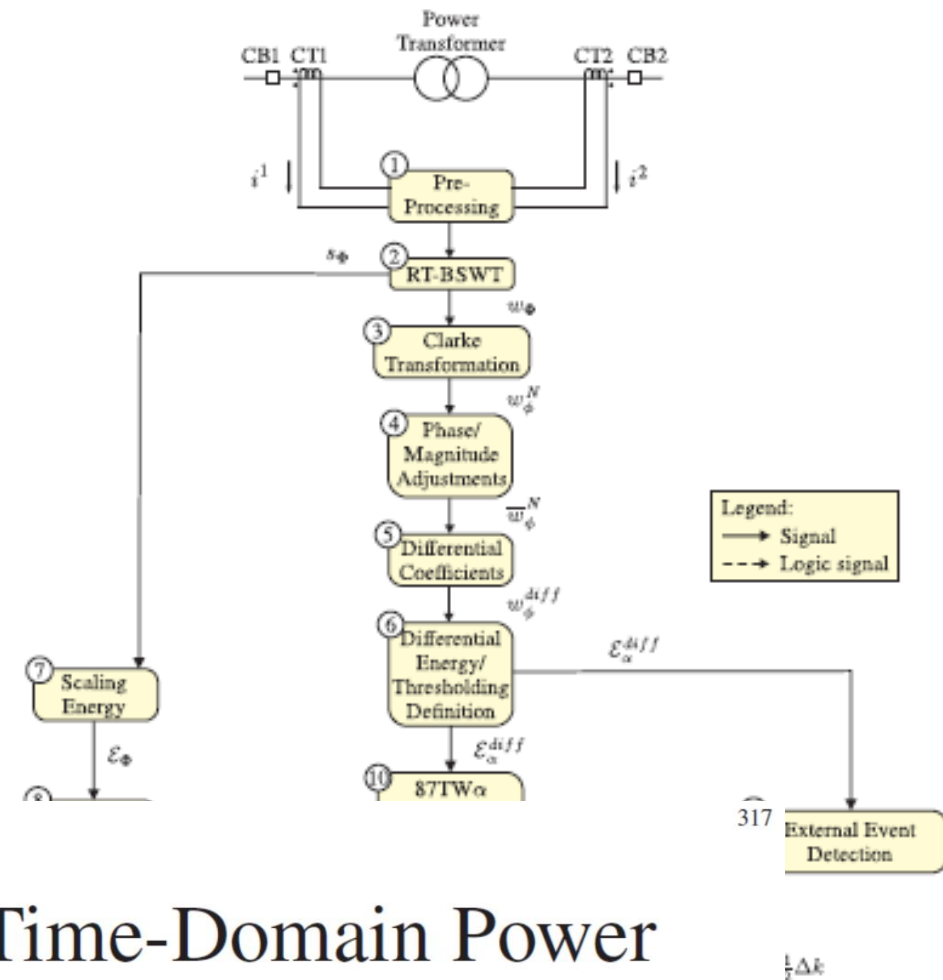
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Mexico








This presentation

- Introduction
- Problem statement
- Developing and results
- Conclusions

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A Clarke-Wavelet-Based Time-Domain Power Transformer Differential Protection

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↓ Trip

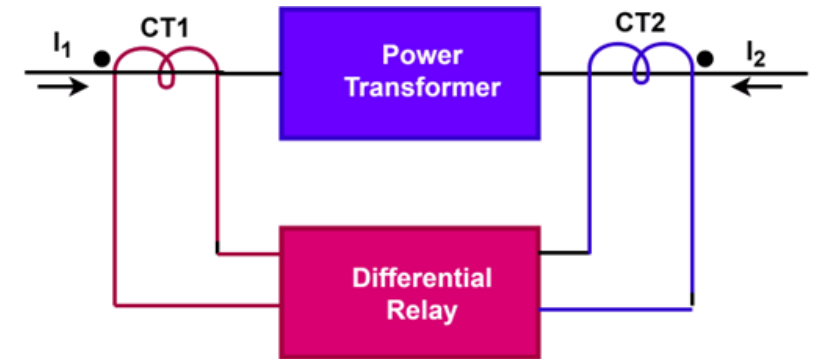
Introduction

- Power transformers are essential in power systems for several key reasons:
 - **Voltage scaling up/down:** step-up or step-down voltage levels
 - **Voltage control:** regulates the voltage with the tap changer
 - **Load Balancing:** enables load distribution by connecting different parts of the electrical grid
 - **Flexibility in power supply:** allows integration of different types of energy sources, such as renewable energy (solar, wind) and traditional power plants
 - **Safety:** steps down high transmission voltages to safer levels for end users



Problem statement

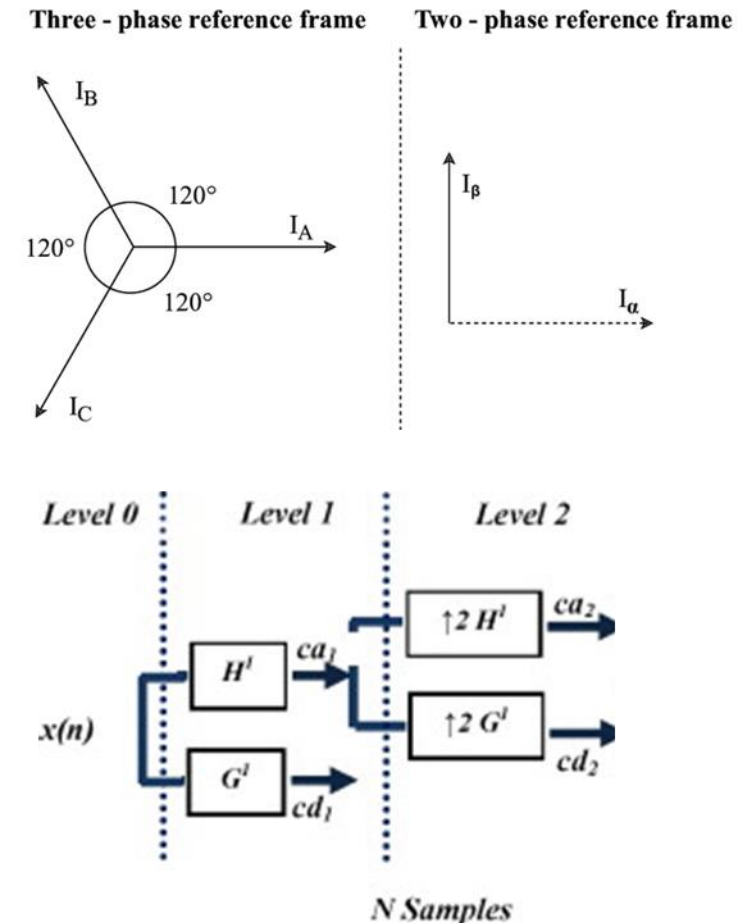
- A fast isolation during fault is imperative to protect the system and the transformer itself
- Commonly, because of its characteristics, **DIFFERENTIAL PROTECTION** is normally used as a primary transformer protection
 - While effective, it must account for diverse situations such as transformer tap changers, CT saturation, overexcitation, and inrush currents
 - Normally, blocking methods enhance the security of the differential protection but may delay internal fault detection and can fail during inrush conditions
 - AI, digital signal processing, and probability theory have been explored to improve protection schemes. Even though they are useful, they increase the computational burden



Differential Protection Scheme

Proposed method

- The Proposed method is based partly on Clarke transform
 - Simple transform, low computational burden
 - it is sensitive and facilitates internal fault detection
 - deals with specific fault types and CT saturation.
- and partly on Wavelet transform,
 - improves detection speed
 - improves accuracy by analyzing high-frequency components



Clark-Wavelet differential protection

Preprocessing

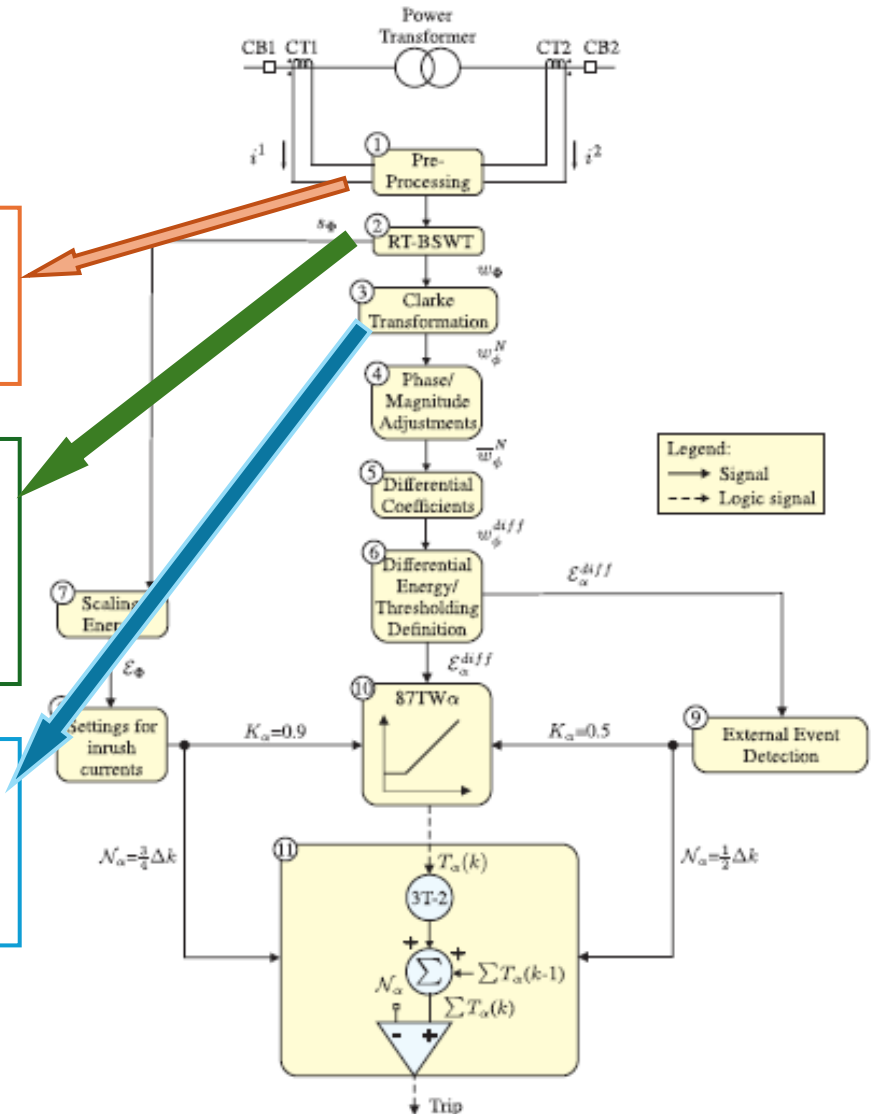
- Acquisition of three-phase CT secondary currents processed by anti-aliasing filters and converter from analogic to digital signal

Real-time boundary stationary wavelet transform RT-BSWT

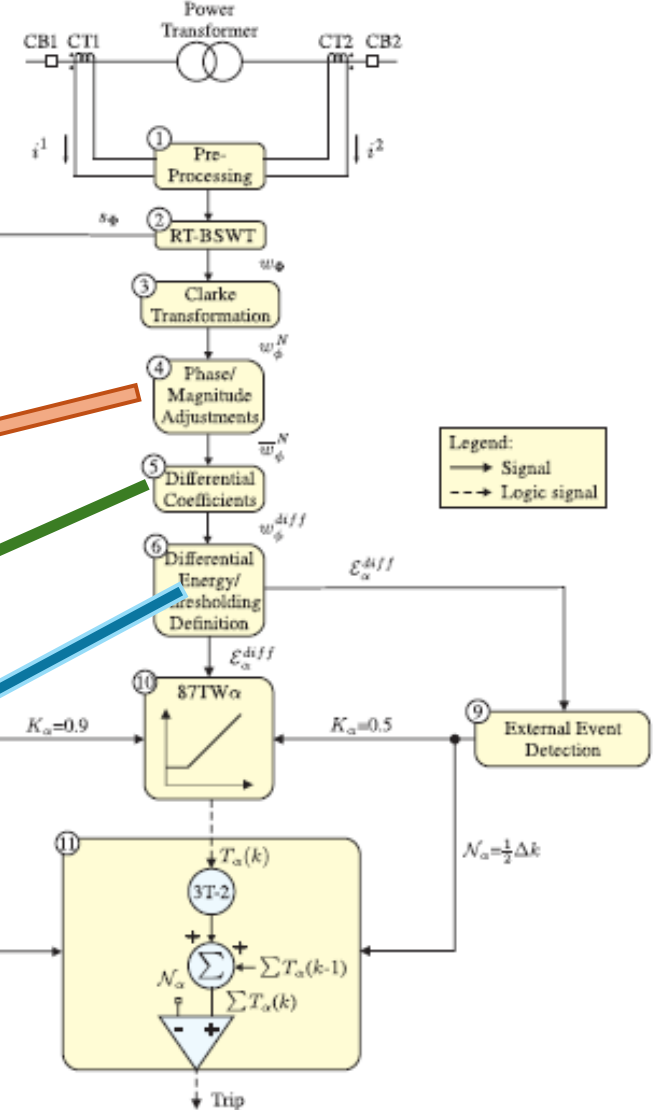
- Scaling and wavelet coefficient
- $s_{\Phi}(l, k) = \frac{1}{\sqrt{2}} \sum_{n=0}^{L-1} h_{\Phi}(n) i_{\Phi}(k - L + n + 1 + l)$
- $w_{\Phi}(l, k) = \frac{1}{\sqrt{2}} \sum_{n=0}^{L-1} h_{\Psi}(n) i_{\Phi}(k - L + n + 1 + l)$

Clark transform

$$\begin{bmatrix} w_{\alpha A}^N(k) \\ w_{\alpha B}^N(k) \\ w_{\alpha C}^N(k) \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & -1/2 & -1/2 \\ -1/2 & 1 & -1/2 \\ -1/2 & -1/2 & 1 \end{bmatrix} \begin{bmatrix} w_A^N(k) \\ w_B^N(k) \\ w_C^N(k) \end{bmatrix}$$



Clark-Wavelet Differential protection



Phase/Magnitude Adjustments

$$\begin{bmatrix} \bar{w}_{\alpha A}^N \\ \bar{w}_{\alpha B}^N \\ \bar{w}_{\alpha C}^N \end{bmatrix} = \frac{1}{TAP_N} M_N \begin{bmatrix} w_{\alpha A}^N \\ w_{\alpha B}^N \\ w_{\alpha C}^N \end{bmatrix}$$

Differential Wavelet Coefficients

$$w_{\phi}^{op}(l, k) = \sum_{m=1}^N \bar{w}_{\phi}^m(l, k)$$

Differential Energy and Automatic Threshold Definition

$$E_{\alpha}^{diff} = \frac{P}{k_2 - k_1 + 1} \sum_{n=k_1}^{k_2} \varepsilon_{\alpha}^{diff}(n)$$

Proposed Clark-Wavelet Differential

Scaling Coefficient Energy

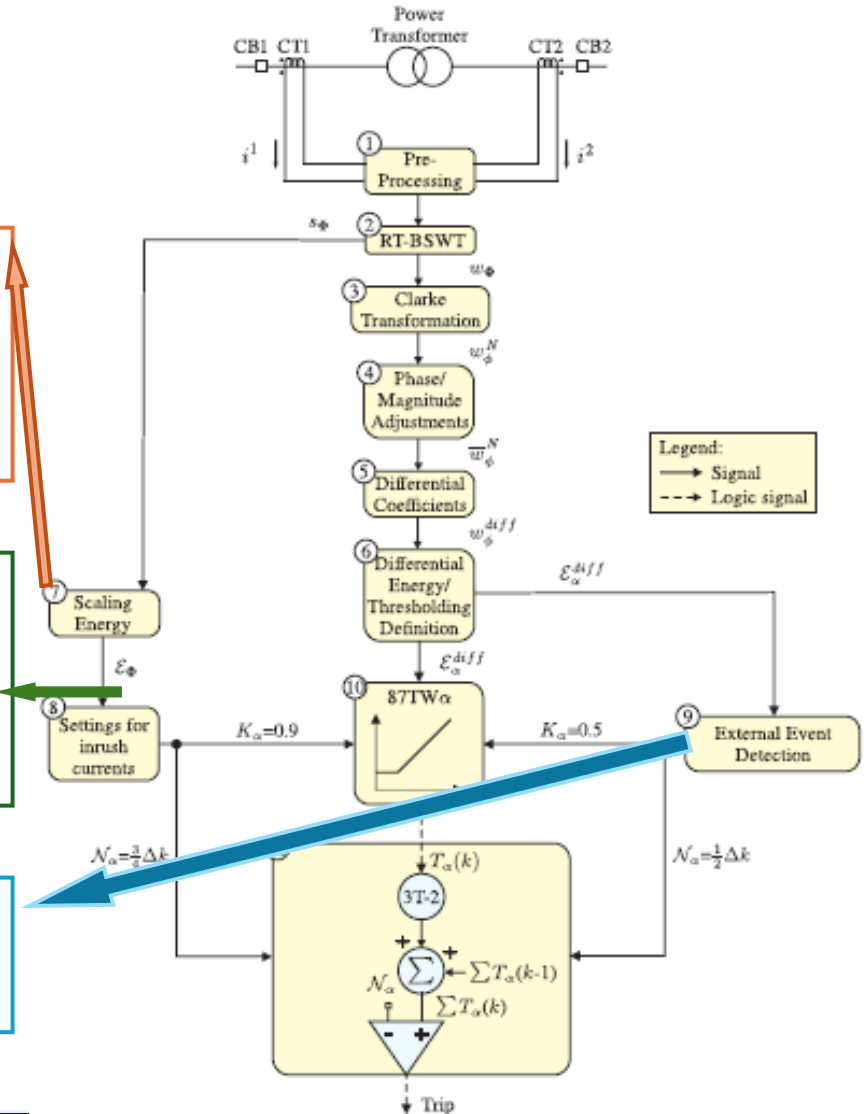
- scaling coefficient energy of the currents are directly proportional to low-frequency components, which is ideal to identify null-currents before transformer energization

Settings for Inrush Currents

- transformer can be identified as opened when currents are lower than the pickup values, accomplished in the wavelet domain as follows $\varepsilon_{\Phi}(k) < E_{\Phi}$

Inception Time Detection of External Events

- Based on energy $\varepsilon_{\alpha}^{op}(k) < K_{\alpha} \varepsilon_{\alpha}^{res}(k)$



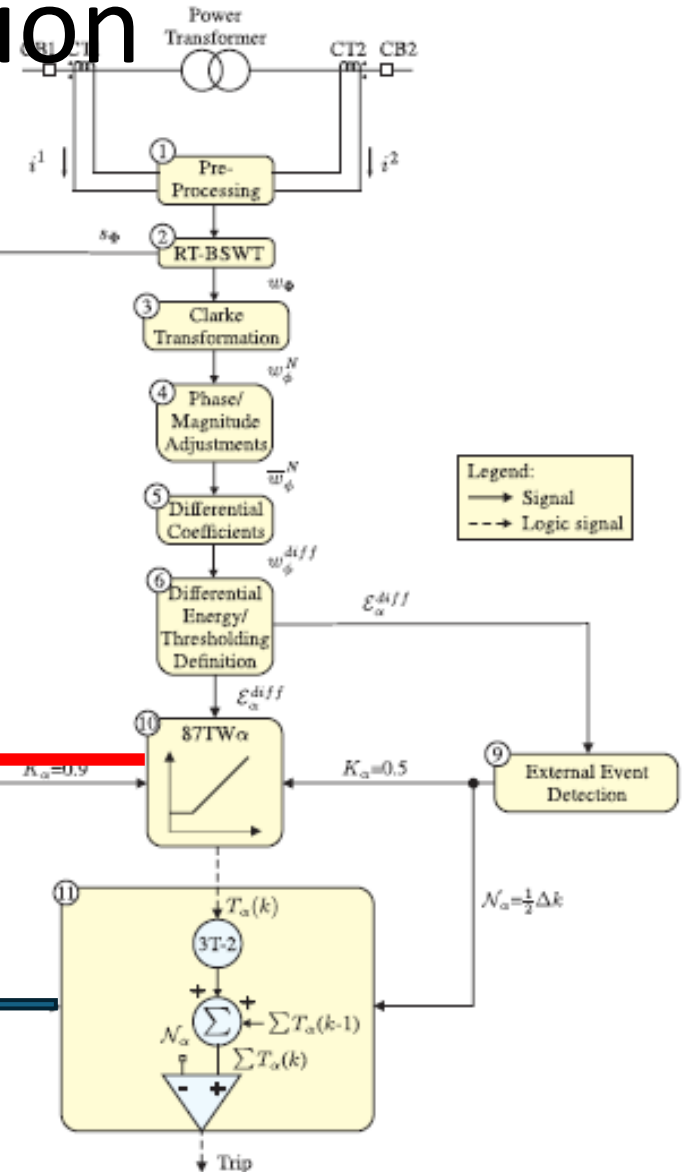
Clark-Wavelet Differential protection

Differential protection unit

- Internal fault if

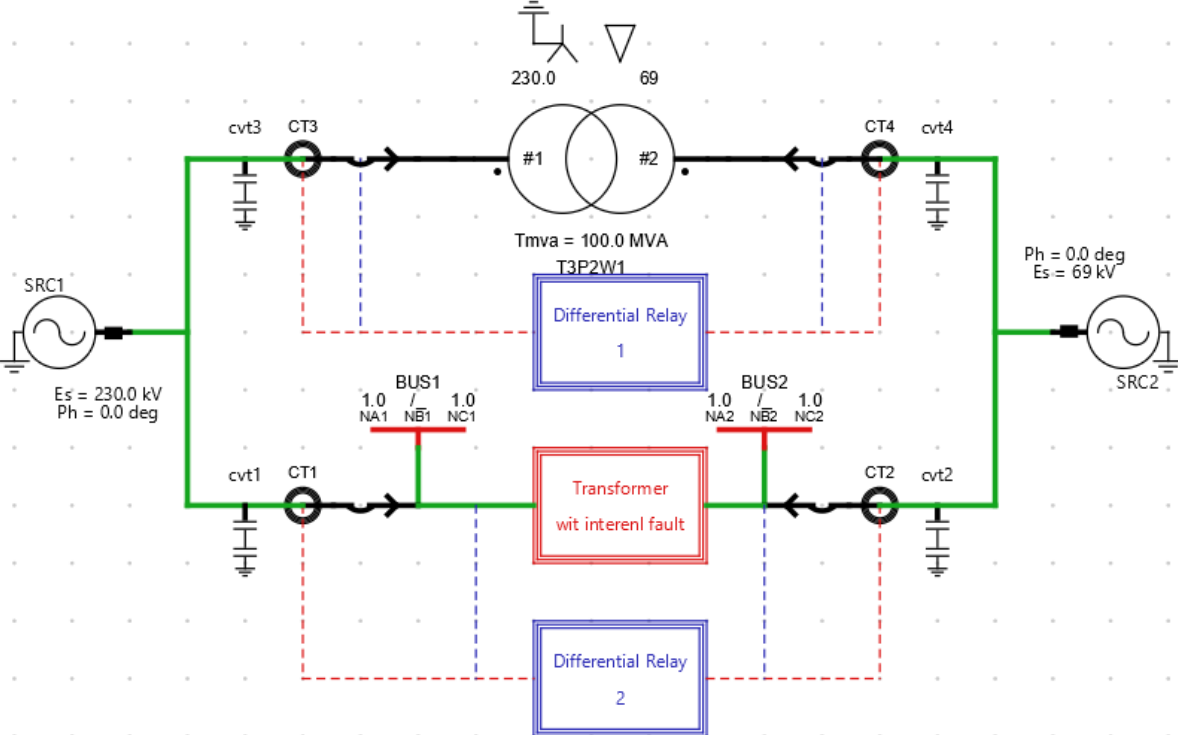
$$\left\{ \begin{array}{l} \varepsilon_{\alpha}^{op}(k) > K_{\alpha} \varepsilon_{\alpha}^{res}(k) \\ \varepsilon_{\alpha}^{op}(k) > E_{\alpha}^{op} \end{array} \right. \text{ and } \left\{ \begin{array}{l} \varepsilon_{\alpha}^{op}(k-1) < E_{\alpha}^{op} \\ \varepsilon_{\alpha}^{res}(k-1) < E_{\alpha}^{res} \end{array} \right.$$

Trip Management

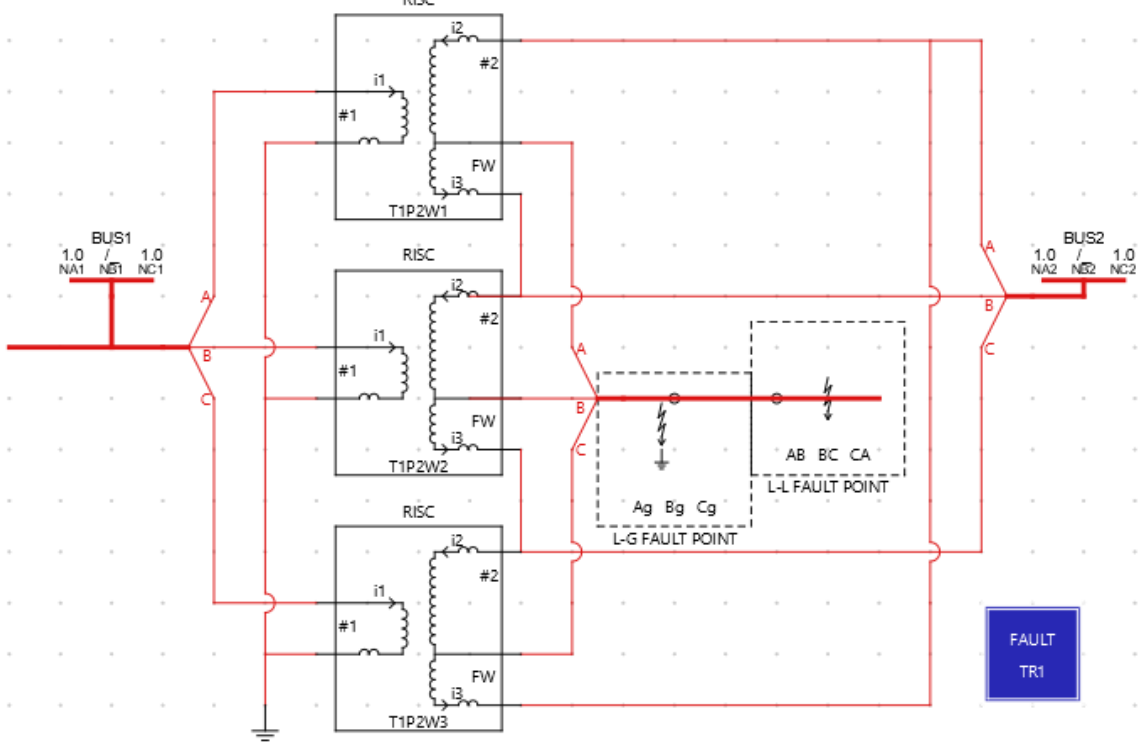


RTDS implementation

- Study case RSCAD Draft

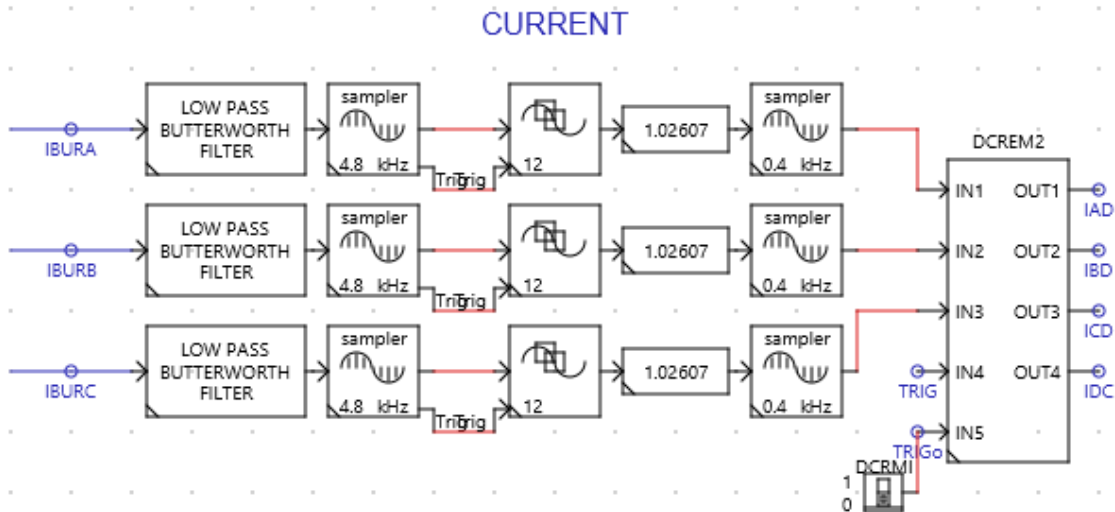


- YgD transformer internal fault

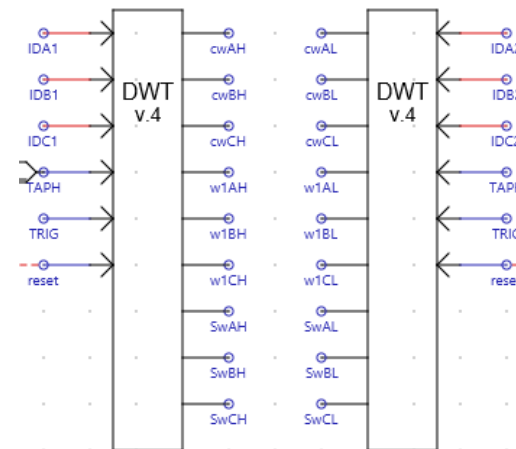


RTDS implementation (1)

- 1st Analog to digital



- 2nd Real time boundary stationary wavelet



- Cbuilder 2.0

- Code

```

***** TASK HEAD *****
TASK NAME : WP4.4
FUNCTION  : avelet_energy
PROJECT   : MIGRATE
AUTHORS   : J. Chavez & M. Popov
           : TUDELFT
           : Mekelweg 5, 2628 CD Delft The Netherlands
ASSUME    : nothing
/ERSION   : $Revision: 1.3 09-26-2024$
*****
$SION:
%01
    
```

```

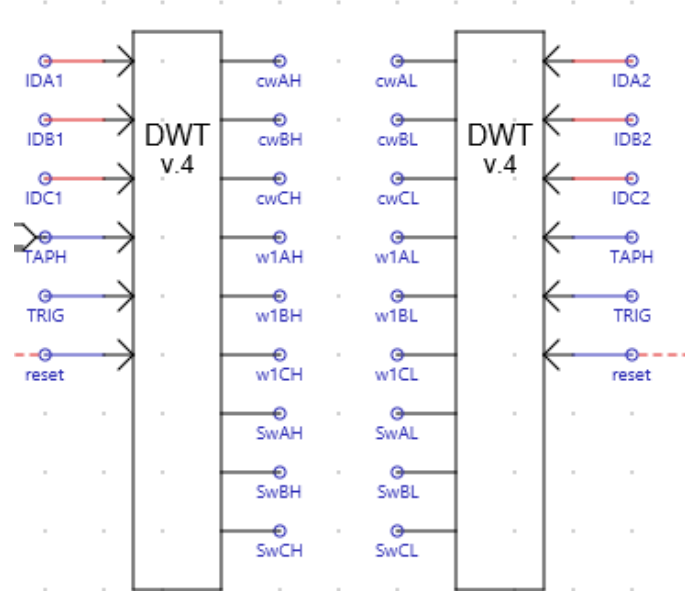
Include file below is generated by C-Builder
// and contains the variables declared as -
// PARAMETERS, INPUTS, OUTPUTS . . .
#include "Wenrgy_V3.h"

STATIC:

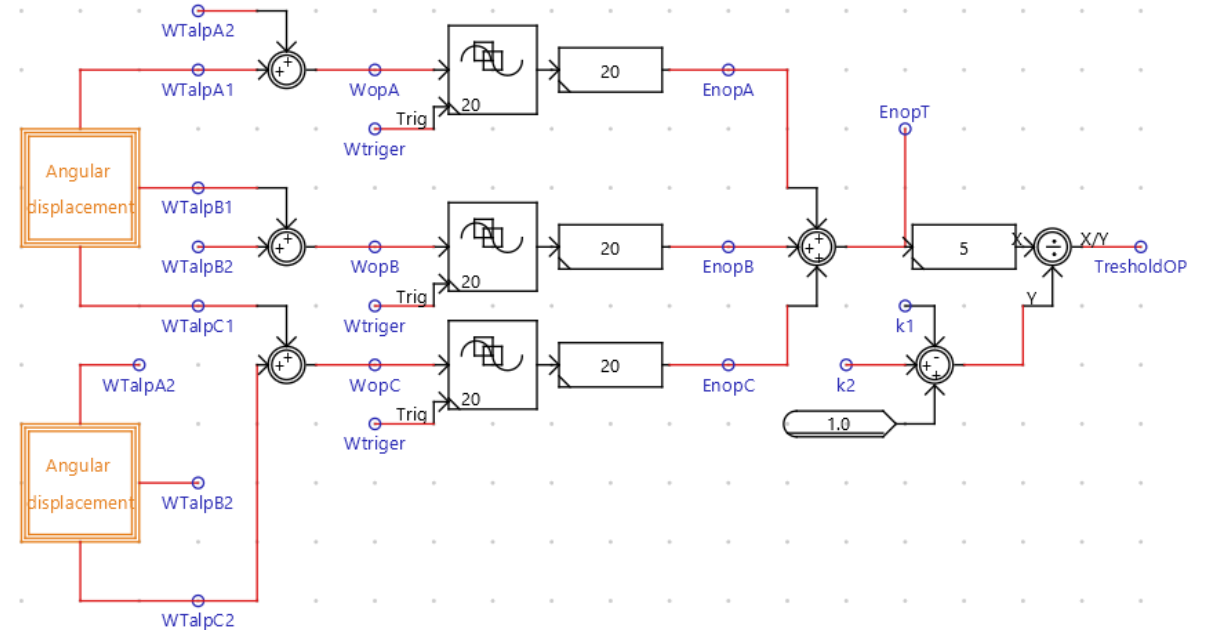
// -----
// Variables declared here may be used in both the
// RAM: and CODE: sections below.
// -----
// double dt;
int N, M, n, k, m, l;
int fd[241]={0,8,4,12,2,10,6,14,1,9,5,13,3,11,7,15,0,8,4,12,2,10,6,14};
    
```

RTDS implementation (2)

- 3th & 4th Clark transform and Real-time boundary stationary wavelet and phase adjustment

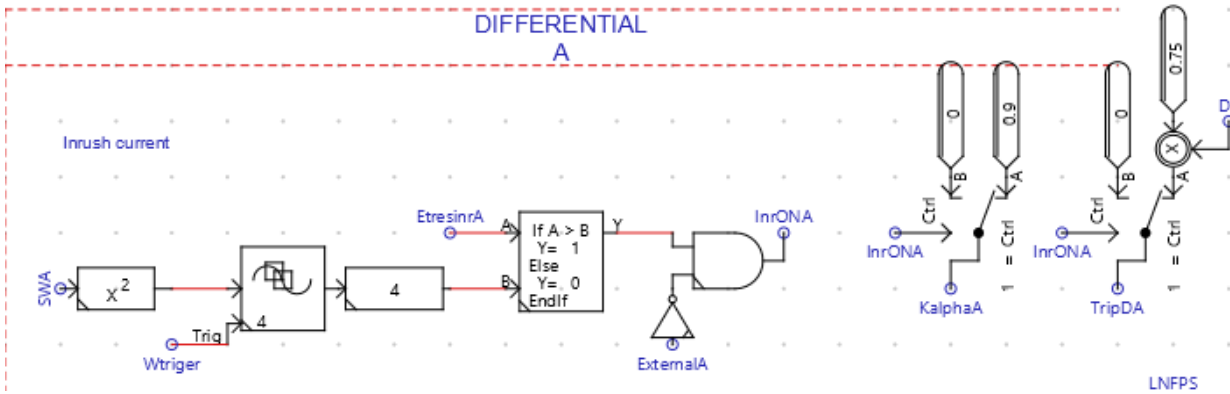


- 6 Differential energy and threshold calculation

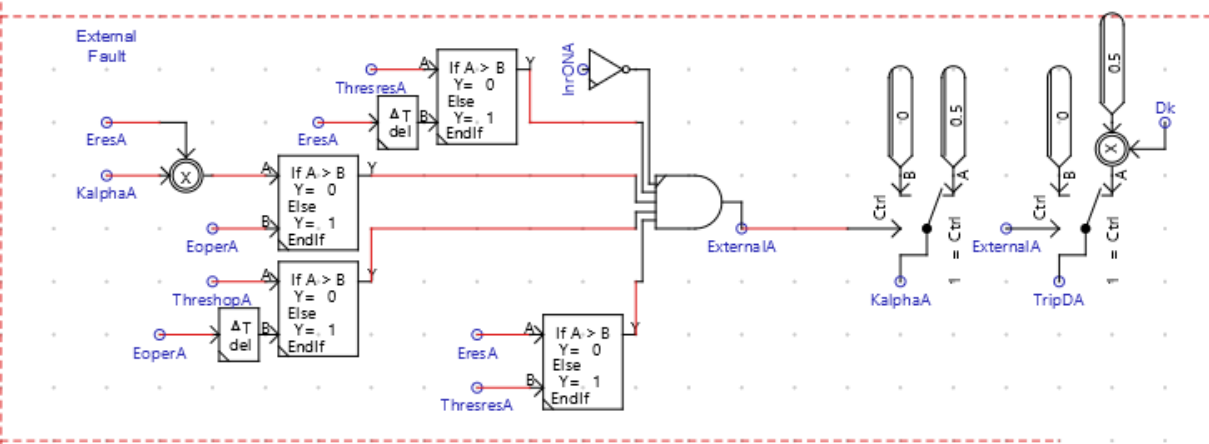


RTDS implementation (3)

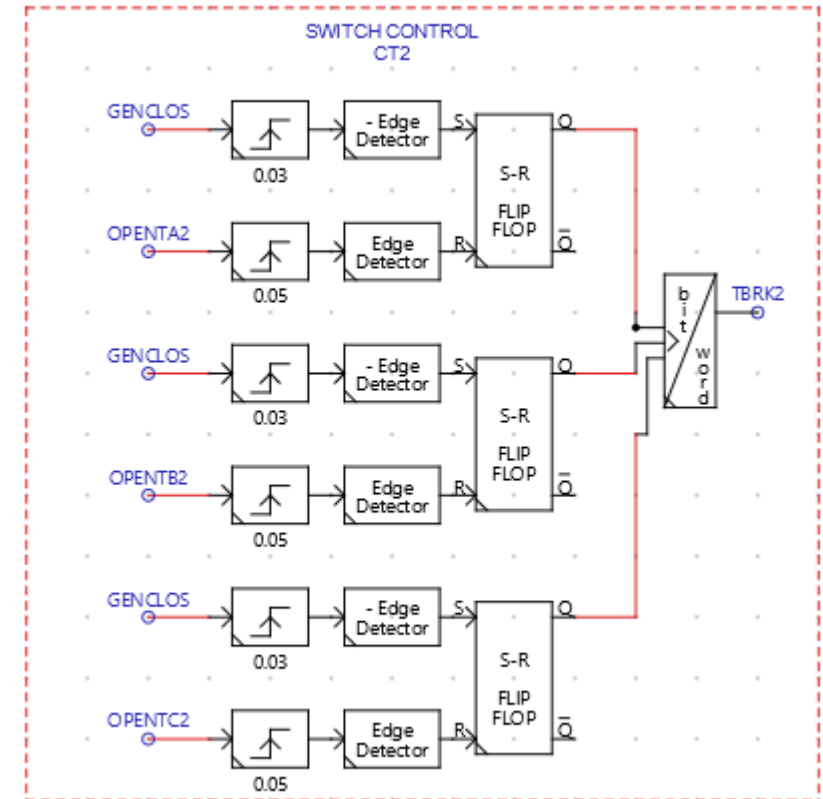
- 7th & 8th Inrush current



- 9th External detection

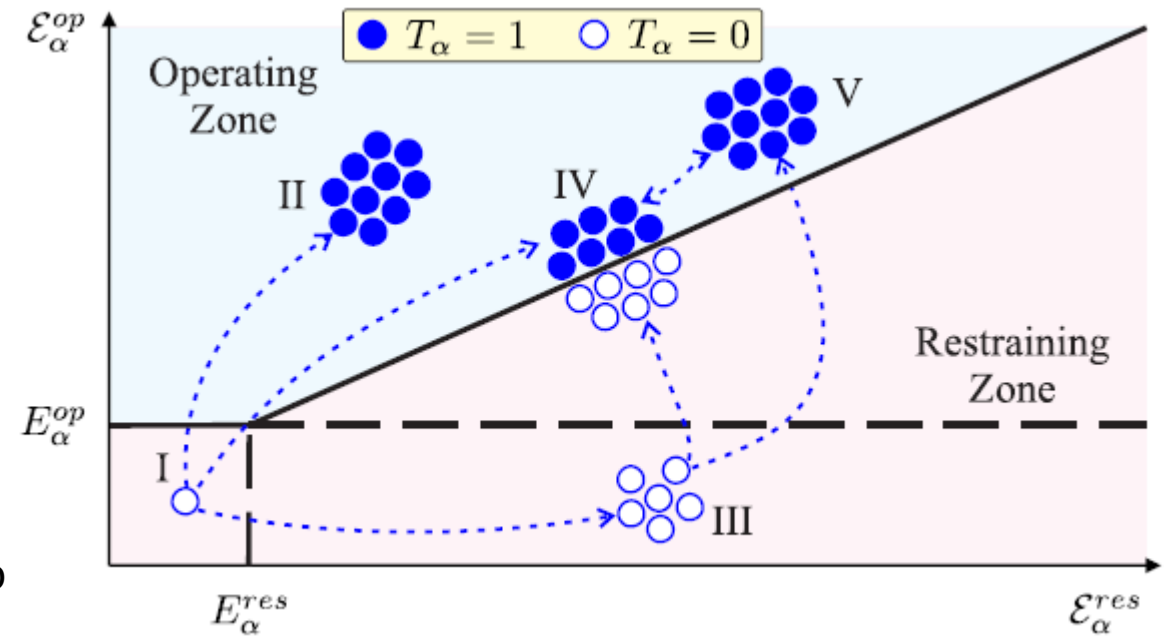


- Breaker control

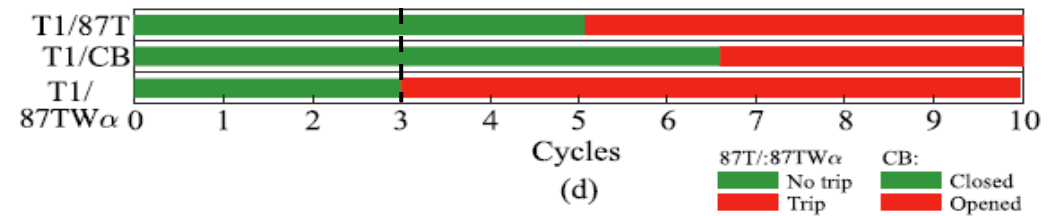
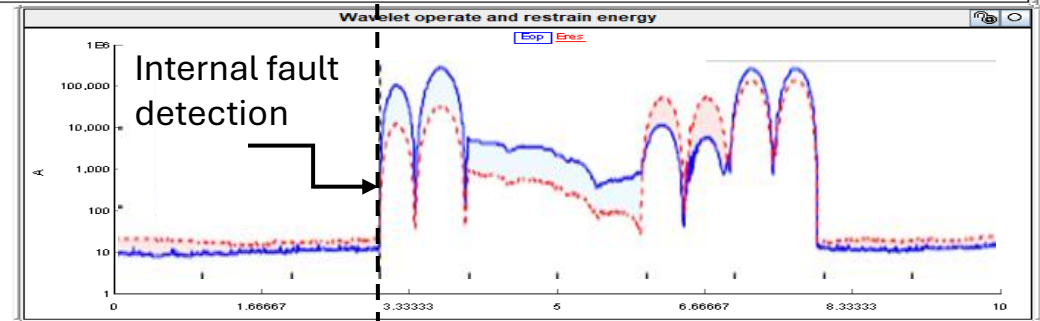
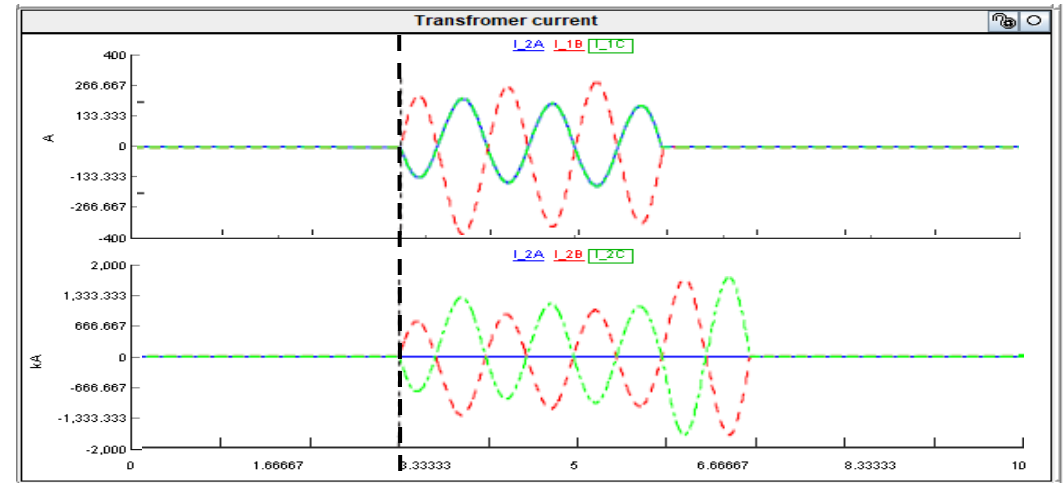
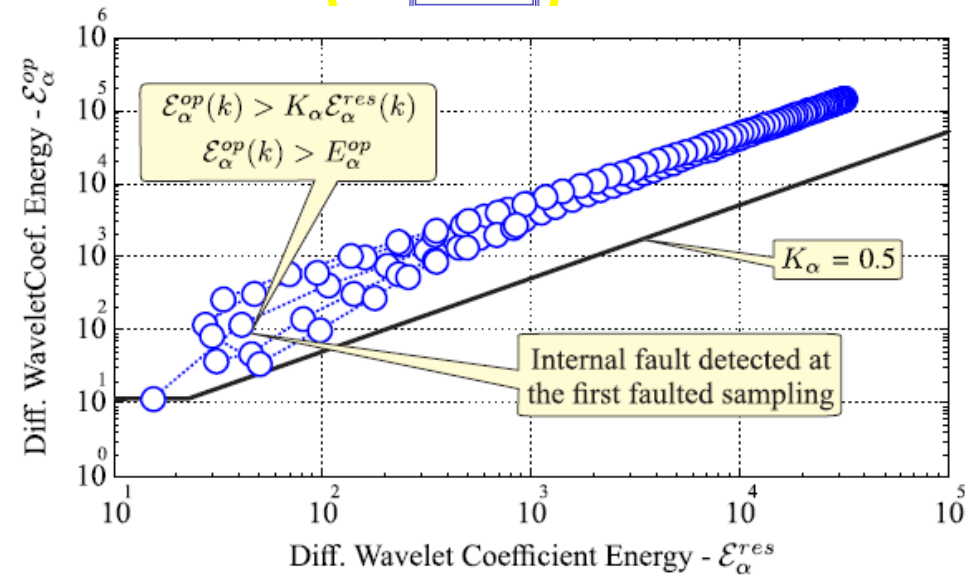
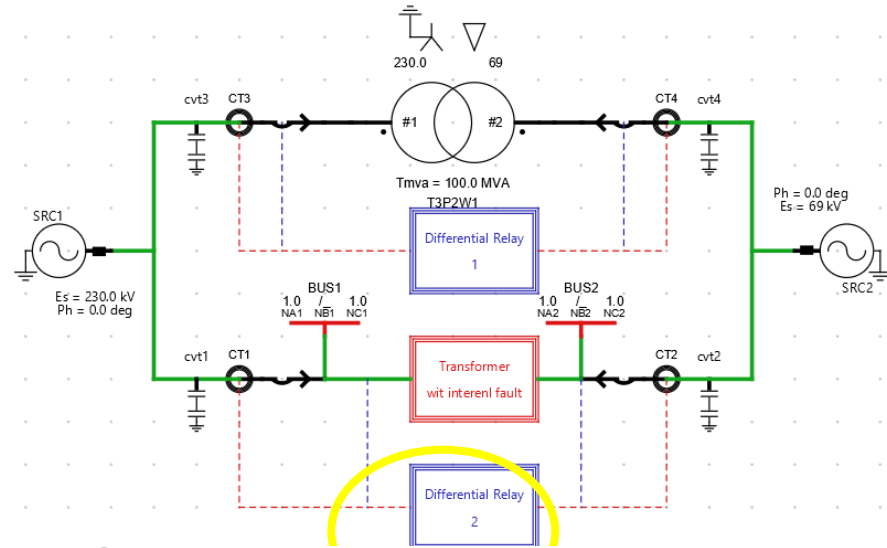


Trajectory of the energy operating points for most of the events

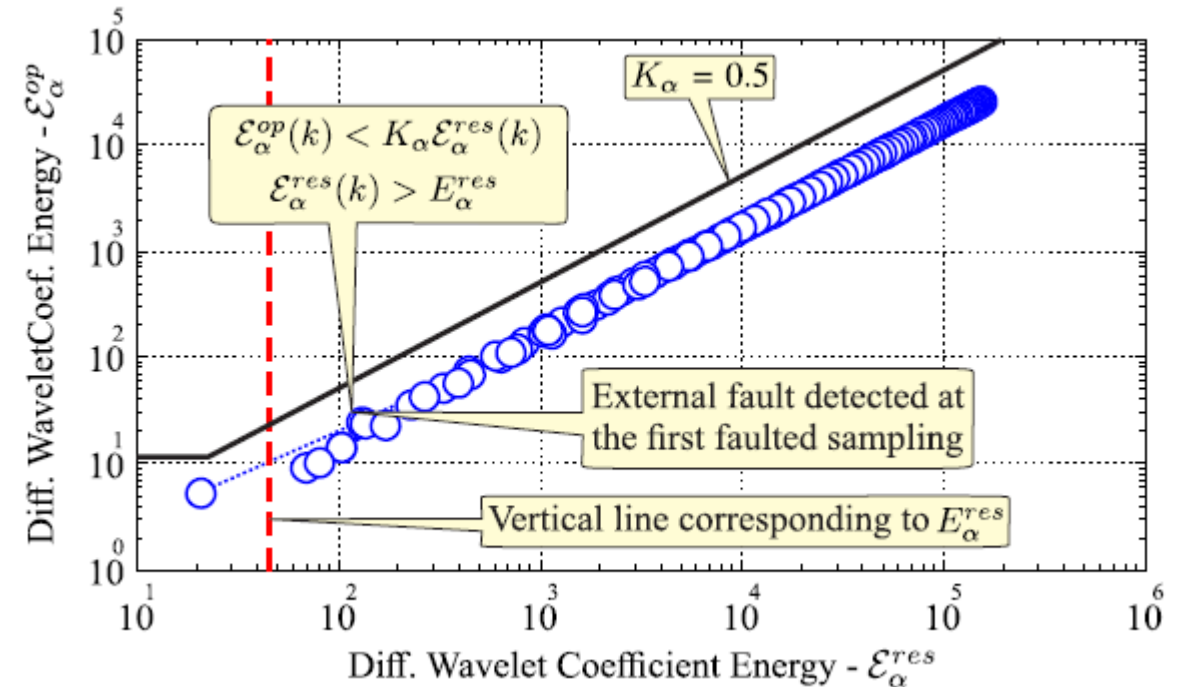
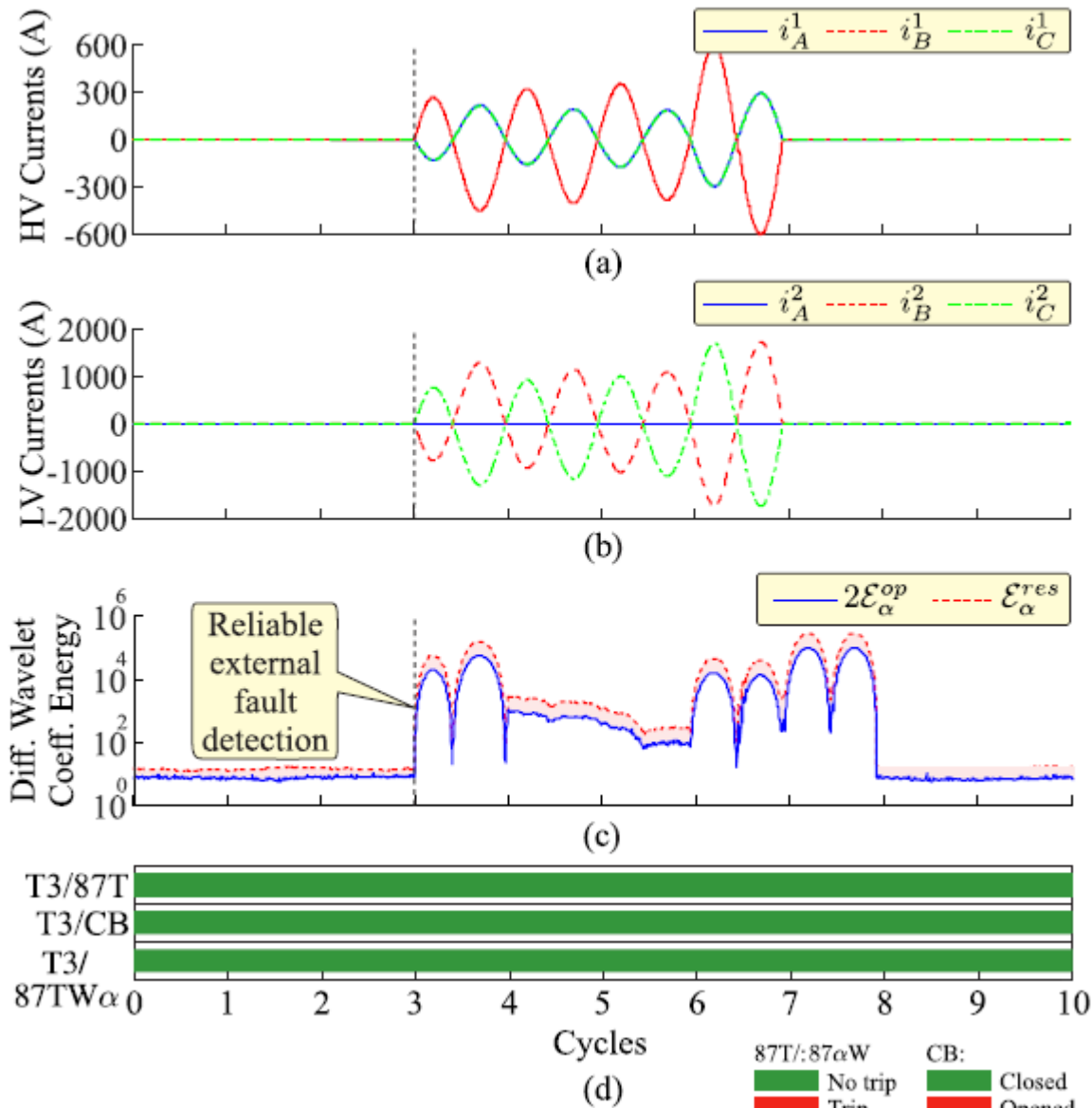
- Steady-state zone I
- Internal fault zone II
- External fault zone III
- External fault followed by CT saturation from I to III and then from III to IV (in the restraining region)
- External fault followed by internal fault from I to III and from III to V
- Overexcitation from I to III and then to IV (in the restraining region)
- Inrush current IV (restraining region)
- Inrush current with permanent fault II
- Inrush current followed by permanent fault from I to IV when the internal fault starts it changes to V



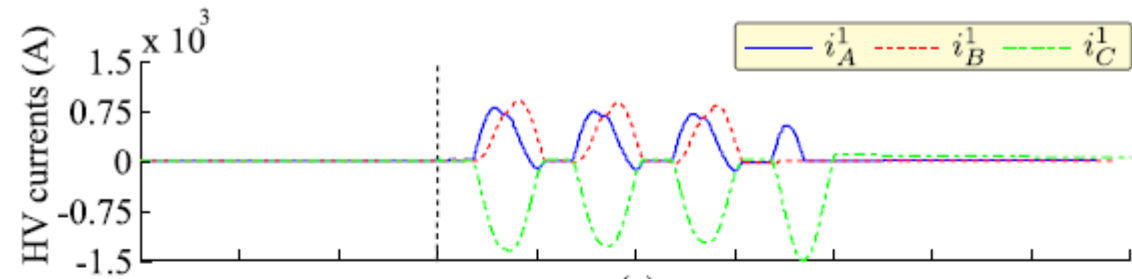
Internal fault A-B



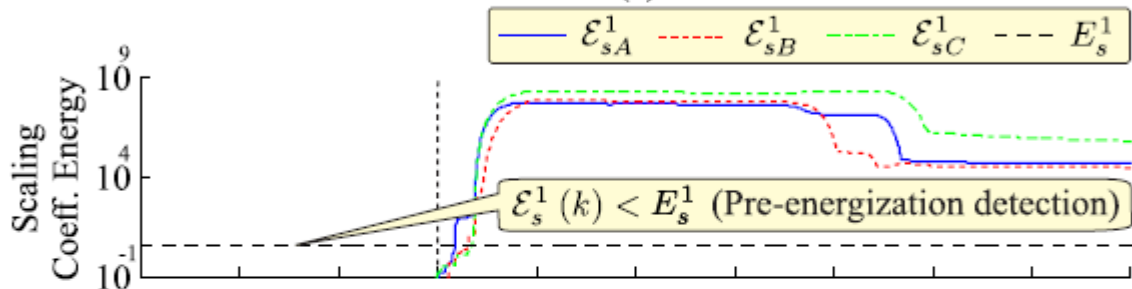
External fault and clearance



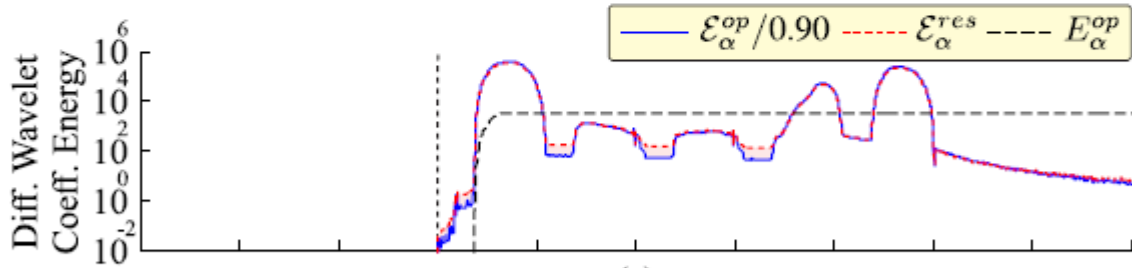
Transformer energization



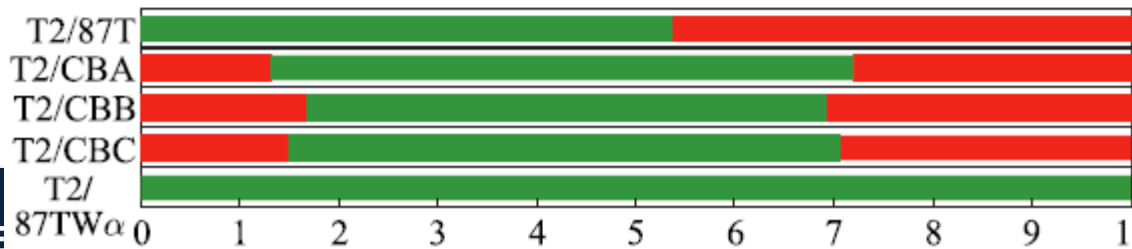
(a)



(b)



(c)



Conclusions

- **Transformer Protection Method:** a time-domain transformer differential protection method using wavelet and Clarke transforms, with a single differential unit (87TW α) that does not require phase segregation or harmonic-based functions.
- **Comparison with Conventional Protection:** The performance of the method was compared to conventional differential protection using both actual and simulated data.
- **Handling Actual Data:**
 - Conventional methods failed during transformer energization due to low harmonic content, resulting in a false trip.
 - The proposed method successfully handled this case in offline analysis.
 - Both methods correctly detected internal faults, but the proposed method was faster, detecting the fault in 65 μ s versus two cycles for the conventional method.
- **Efficiency and Simplicity:** The use of Clarke and wavelet transforms ensures computational efficiency and simplicity, with the equations requiring only addition and multiplication, making hardware implementation feasible.

