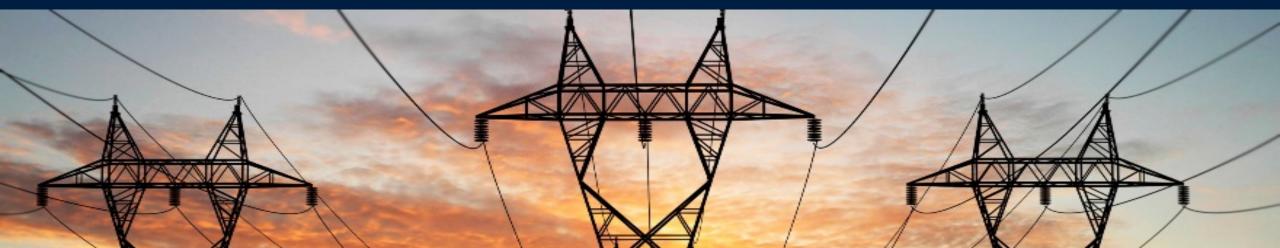
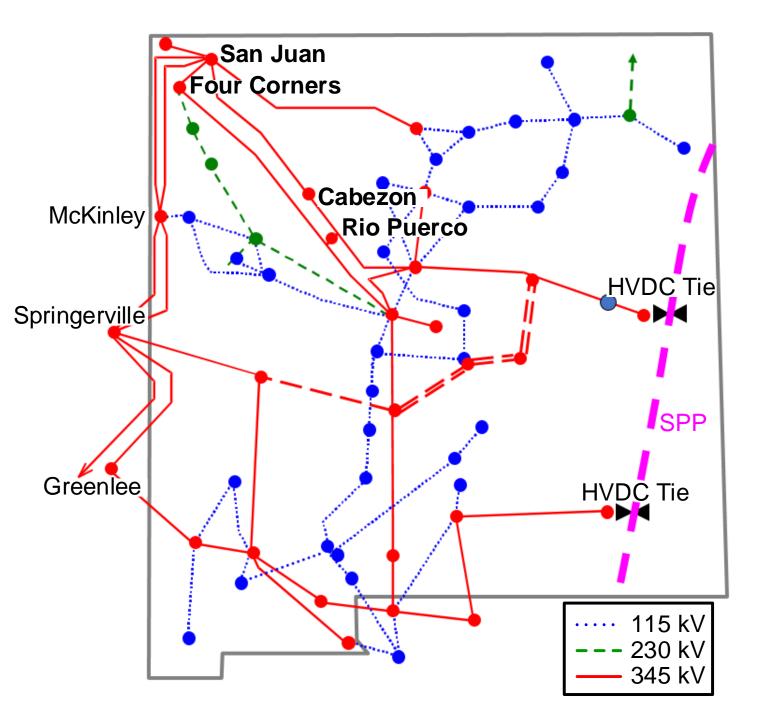


How RTDS and SEL Marked Historic Milestone in Power System Protection

Jordan Bell, P.E. Senior Protection Engineer

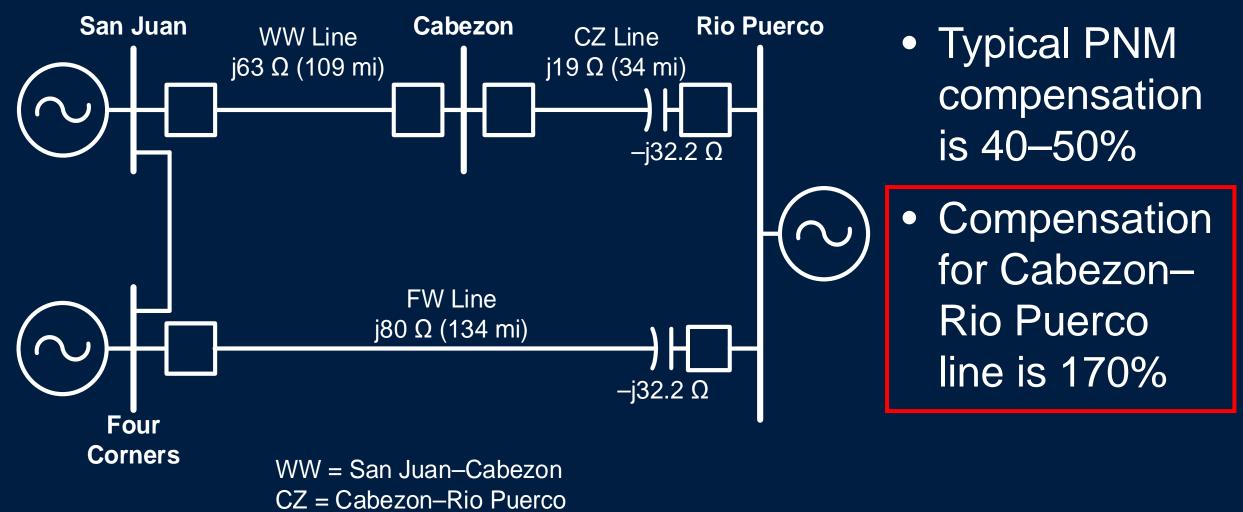




Public Service Company of New Mexico

- 14,388 mi of transmission lines
- 69 345 kV primary voltage
- 46 kV subtransmission
- Large generation at San Juan and Four Corners substations

Cabezon Project Summary



FW = Four Corners–Rio Puerco

Public Service Company of New Mexico (PNM) Transmission Challenge

- 345 kV line split by new substation
- Series capacitor near one end
- Shorter part overcompensated $X_L X_C < 0$
- Challenge for traditional protection
- Simple for the SEL-T400L i = C dv / dt dv = i / C dt
- dt is so short, it is like the capacitor is not even there!

PNM's Protective Relays Standard



Phasor-Based

• 87L

- 21P / G Quadrilateral
- 67P/G



- Time-Domain
 - TW87 / TW32
 - TD21 / TD32

Phasor and Time-Domain Principles Similarities and Differences

Algorithm	Phasors		
Signal Spectrum of Interest	40–70 Hz		
Filtering			
Sampling	8 / cycle		
Line theory	$V_F = V - ZI$		
Operating time	1 cycle		
CT and PT requirements	Low		

Ultra-High-Speed Line Protection Offered by Time-Domain Elements and Schemes

- Based on traveling waves
 - Differential scheme, TW87, 1–3 ms
 - Directional element, TW32, 0.1 ms
- Based on incremental quantities
 - Underreaching distance element, TD21, 2–6 ms
 - Directional element, TD32, 1.5 ms

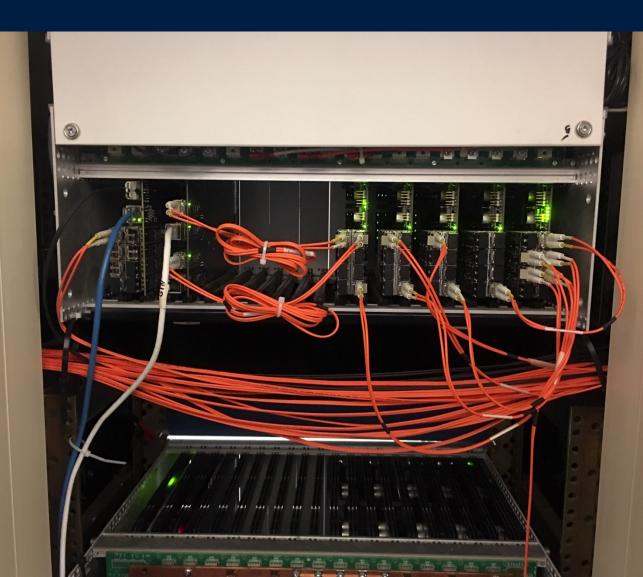
Processing Interval Comparison

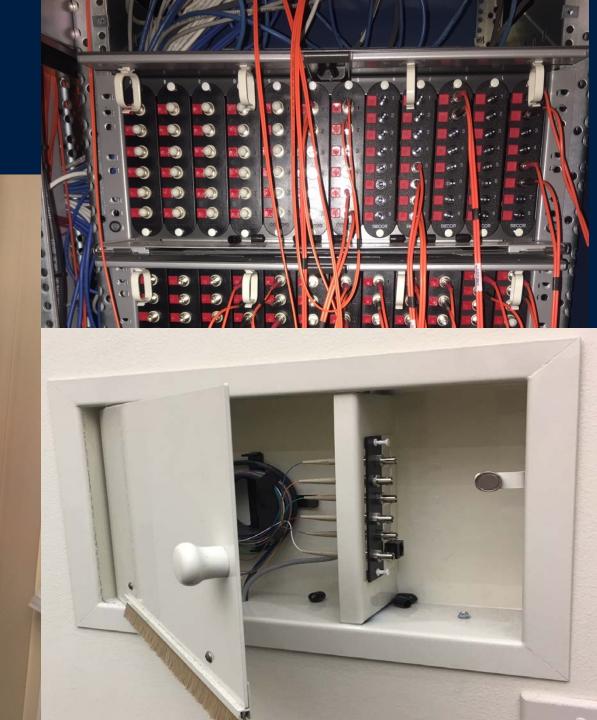
- RTDS time-step: typically 50 µs
- Relay processing intervals
 - Phasor-based: 8 samples per cycle (~2 ms)
 - Incremental quantity calculations: every 100 µs
 - Traveling-wave calculations: every 1 µs

SEL Engineering Services RTDS and Relay Test Setup

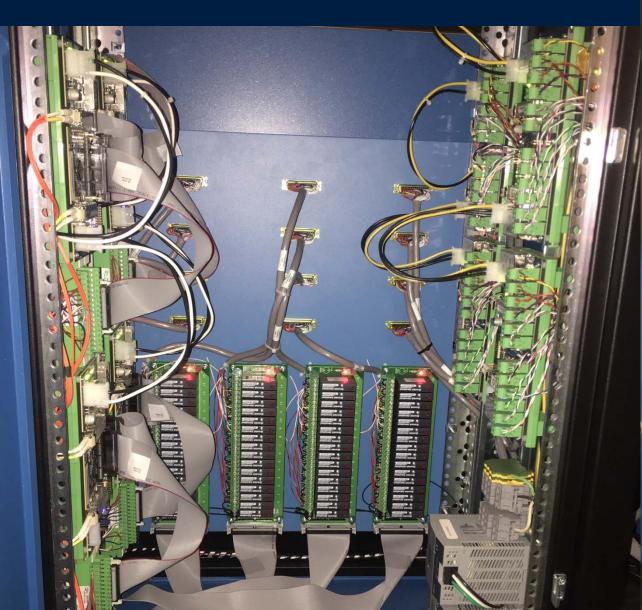


Fiber Connections





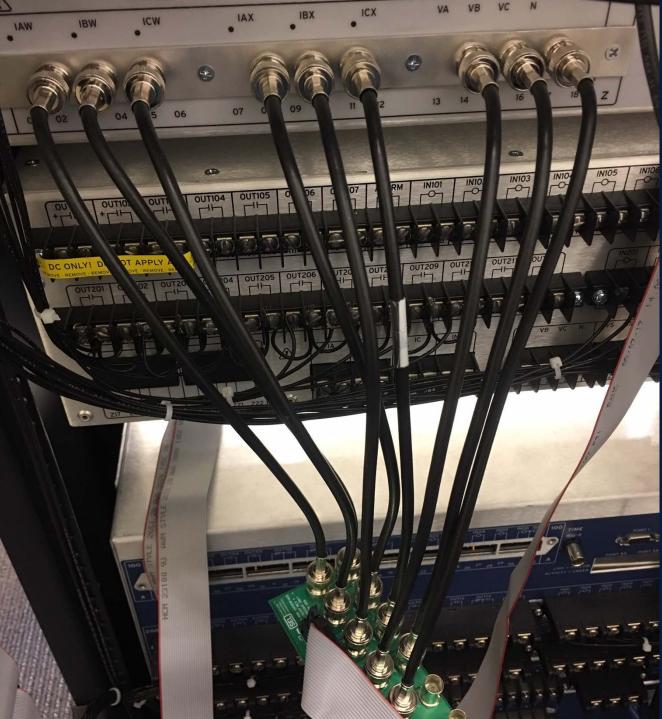
I/O Connections





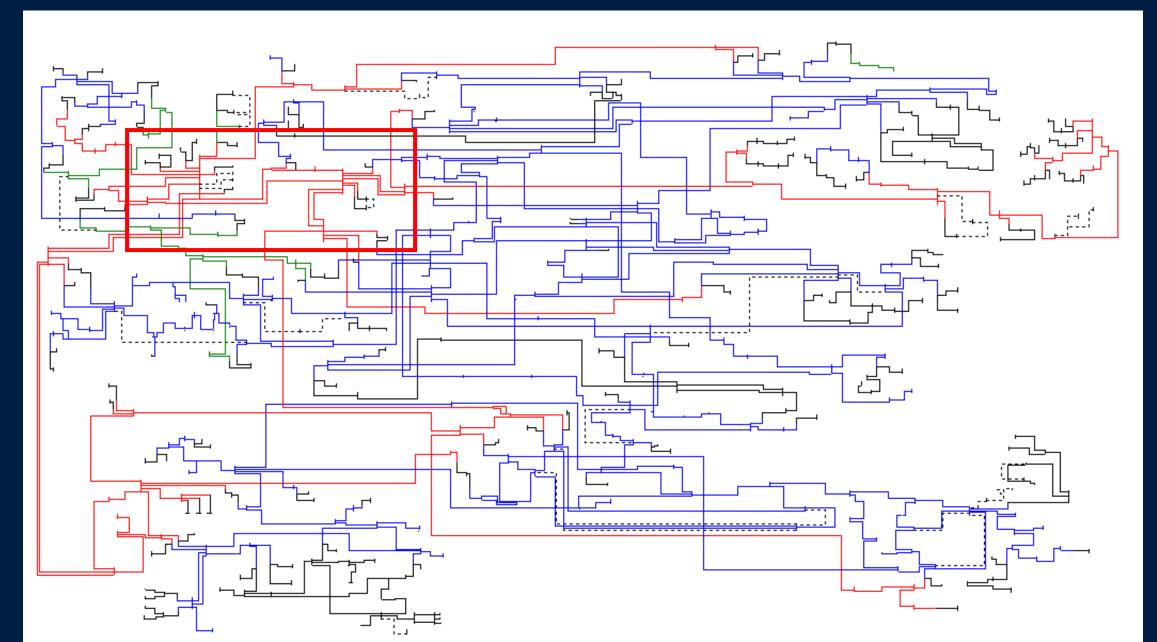
Relay Connections



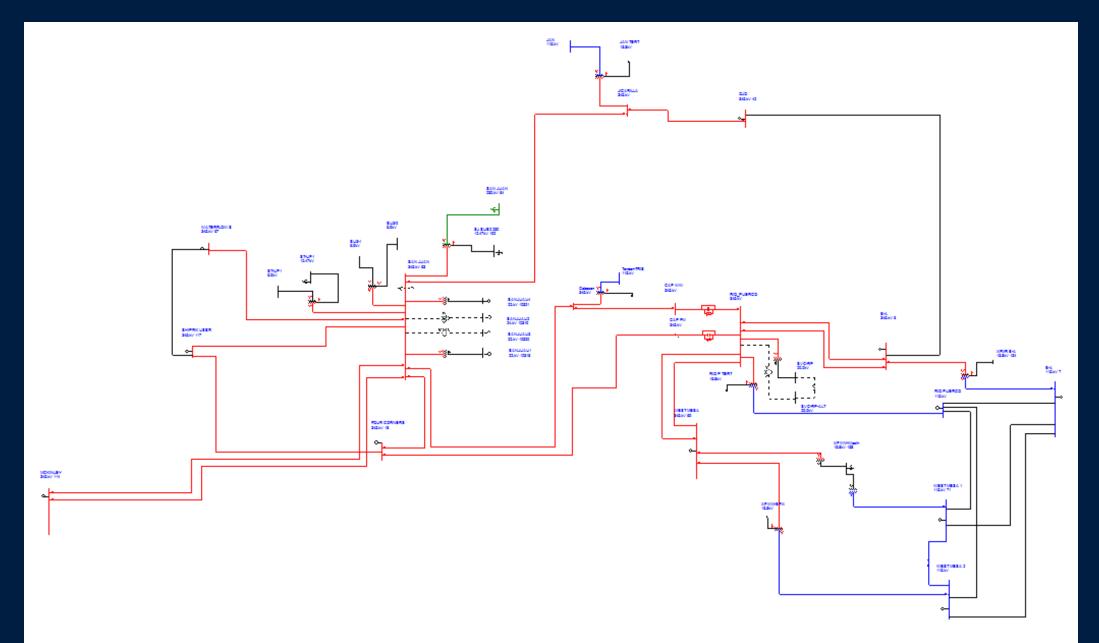


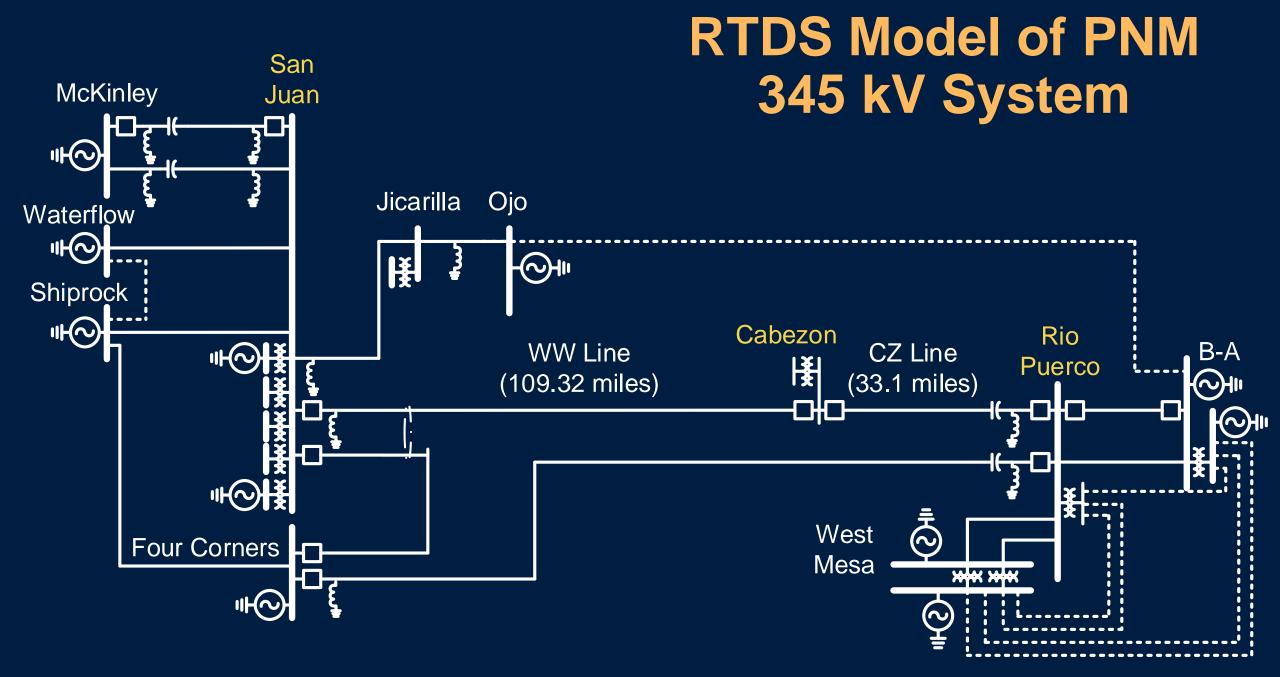
Model Development

Short-Circuit Model



Reduced Short-Circuit Model





Model Validation

Positive-Sequence	Z1_ohms := Z1_source Z1_ang := arg(Z1_source)	$Z1_ohms = 32.71 \Omega$ $Z1_ang = 88.21 \cdot deg$	CAPE: Z1 := $Z_{525} \cdot (0.00097 + j \cdot 0.02434)$ Z0 := $Z_{525} \cdot (0.01264 + j \cdot 0.08735)$ Z0M := $Z_{525} \cdot (0.0112 + j \cdot 0.0436)$)	
Zero-Sequence:	Z0_source := Z ₅₂₅ ·(0.00035 + j·0.01120) Z0_ohms := Z0_source Z0_ang := arg(Z0_source)	Z0_ohms = 30.89 Ω Z0_ang = 88.21·deg	$Z1 = (2.67 + 67.09i) \Omega$ $Z0 = (34.84 + 240.76i) \Omega$ $Z0M = (30.87 + 120.17i) \Omega$	Z1_cape := $ Z1 = 67.14 \Omega$ Z0_cape := $ Z0 = 243.27 \Omega$ Z0M_cape := $ Z0M = 124.074 \Omega$	Z1A_cape := arg(Z1) = 87.72 · deg Z0A_cape := arg(Z0) = 81.77 · deg Z0MA_cape := arg(Z0M) = 75.59 · deg
7.03 (100 MUA)		RTDS: Z1 := $Z_1 \cdot (2.88 + j \cdot 67.33)$ Z_shunt_pos_rtds := $Z_1 \cdot 0 + j \cdot 1246.16 $ Z0 := $Z_1 \cdot (33.93 + j \cdot 246.93)$ Z_shunt_zero_rtds := $Z_1 \cdot 0 + j \cdot 2162.94 $ Z0M := $Z_1 \cdot (31.00 + j \cdot 127.05)$ Z_shunt_zero_rtds := $Z_1 \cdot 0 + j \cdot 2162.94 $			
	$Zps := \frac{7.93}{100} \left(\frac{100 \text{MVA}}{600 \text{MVA}} \right) = 0.01322$ $Zpt := \frac{13.07}{100} \left(\frac{100 \text{MVA}}{100 \text{MVA}} \right) = 0.1307$		$Z1 = (2.88 + 67.33i) \Omega$ $Z0 = (33.93 + 246.93i) \Omega$ $Z0M = (31 + 127.05i) \Omega$	Z1_rtds := $ Z1 = 67.39 \Omega$ Z0_rtds := $ Z0 = 249.25 \Omega$ Z0M_rtds := $ Z0M = 130.78 \Omega$	Z1A_rtds := arg(Z1) = 87.55.deg Z0A_rtds := arg(Z0) = 82.18.deg Z0MA_rtds := arg(Z0M) = 76.29.deg
	$Z_{st} := \frac{8.55}{100} \left(\frac{100 \text{MVA}}{100 \text{MVA}} \right) = 0.0855$		RTDS_Error_pos := $\frac{Z1_rtds - Z1_cape}{Z1_cape}$		RTDS_Error_pos = 0.374.%
			$RTDS_Error_zero := \frac{Z0_rtds - Z0_c}{Z0_c}$ $RTDS_Error_mut := \frac{Z0M_rtds - Z0M_rtds}{Z0M}$	<u>Z0_cape</u> ape - <u>Z0M_cape</u> [_cape	RTDS_Error_zero = 2.46.% RTDS_Error_mut = 5.403.%

Test Procedure and Results

Test Procedure

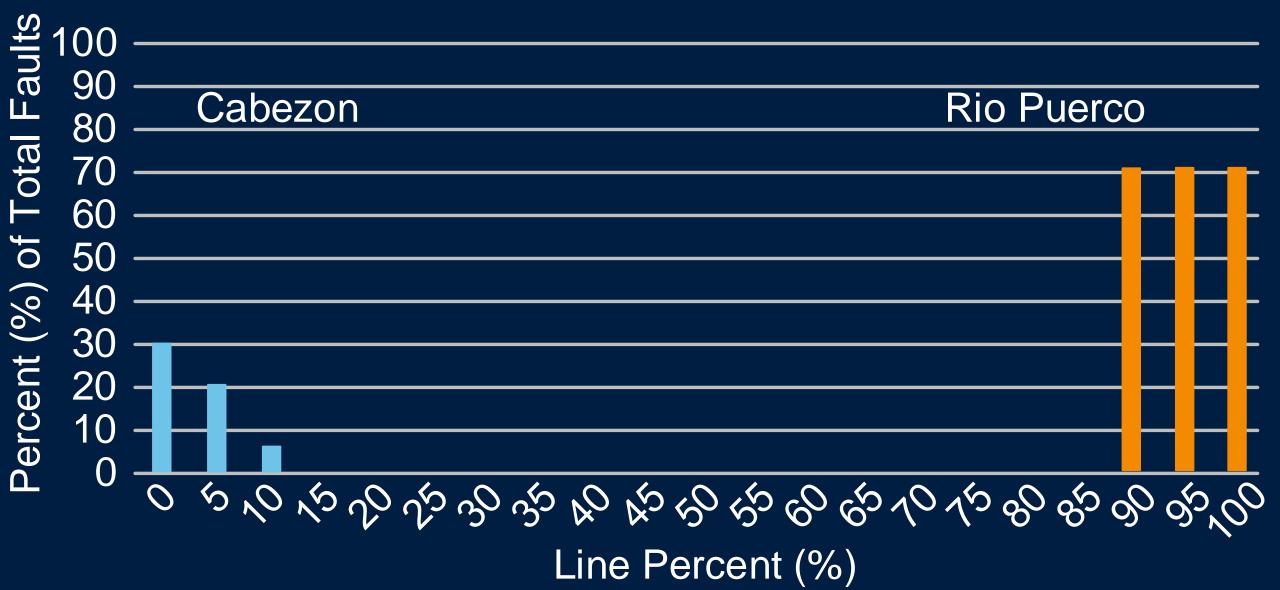
- Internal faults test dependability
- External faults test security
- Fix any issues identified
- Run batch tests
 - All 10 fault types
 - Fault inception angles of 0, 30, 60, 90 degrees
 - All load flow cases (contingencies)

What Did We Get?

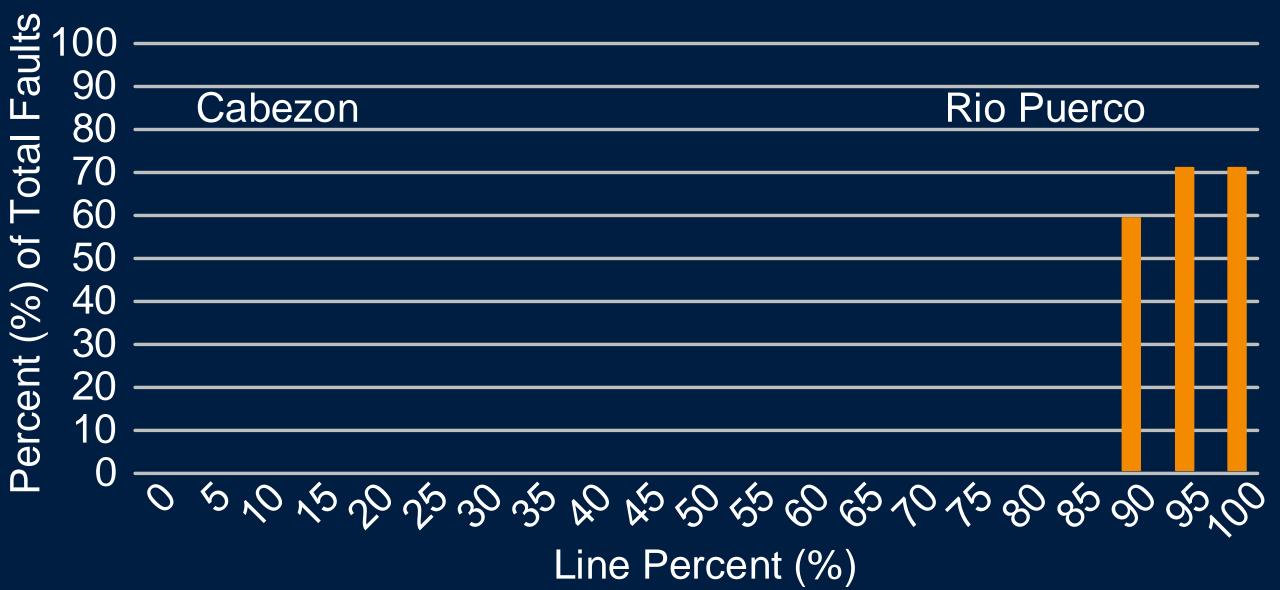
- 22 internal and 26 external locations
- 10,000+ faults applied
- Text files of relay operation times
- COMTRADE and JPEG files of every simulation

CASE	POS	TYPE	POW	LS_TPAT	LS_TPBT	LS_TPCT
LFA	Floc1	_AG	0	0.018479999	0	0
LFA	Floc1	_AG	45	0.018409999	0	0

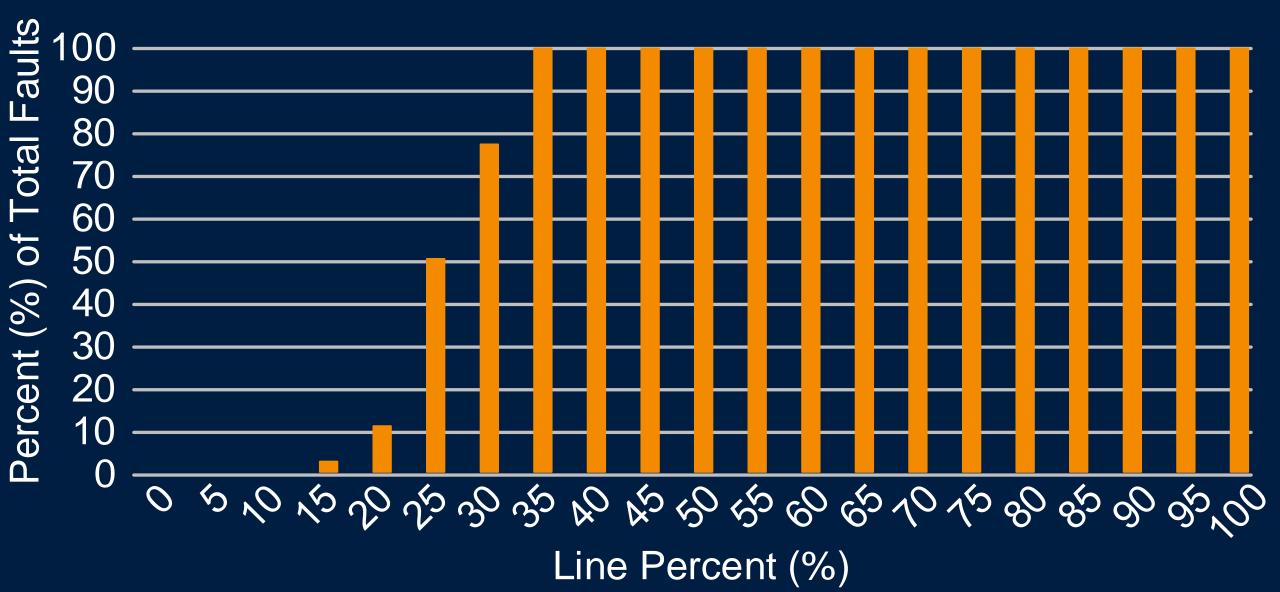
Ground Overcurrent Phasor-Based Protection



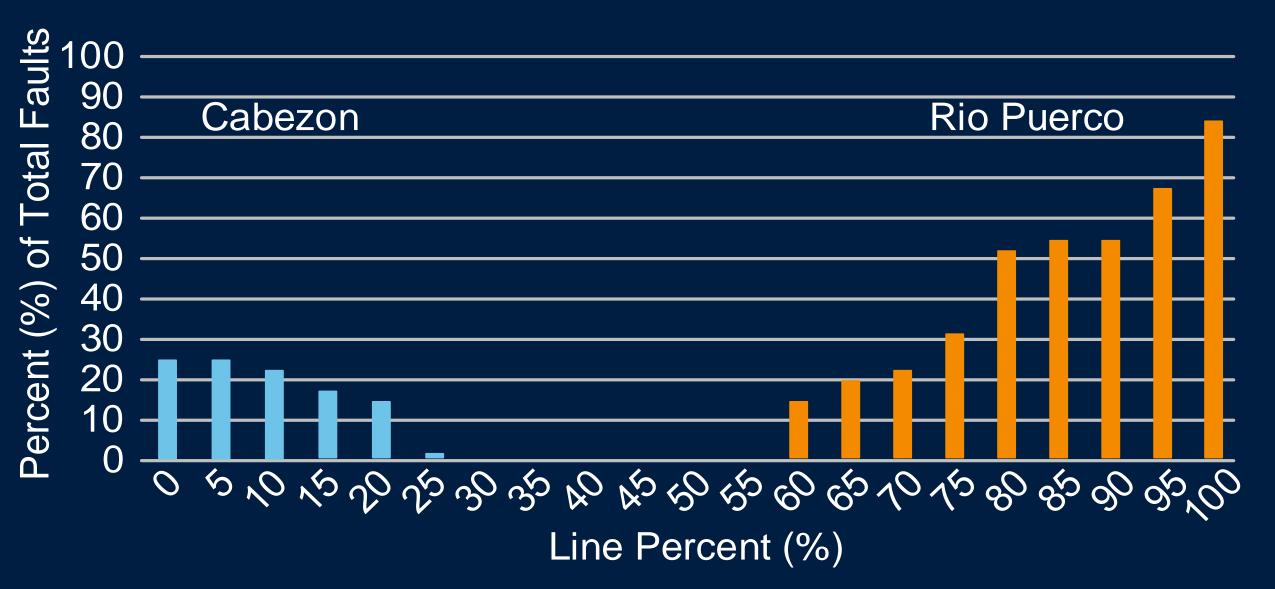
Phase Overcurrent Phasor-Based Protection



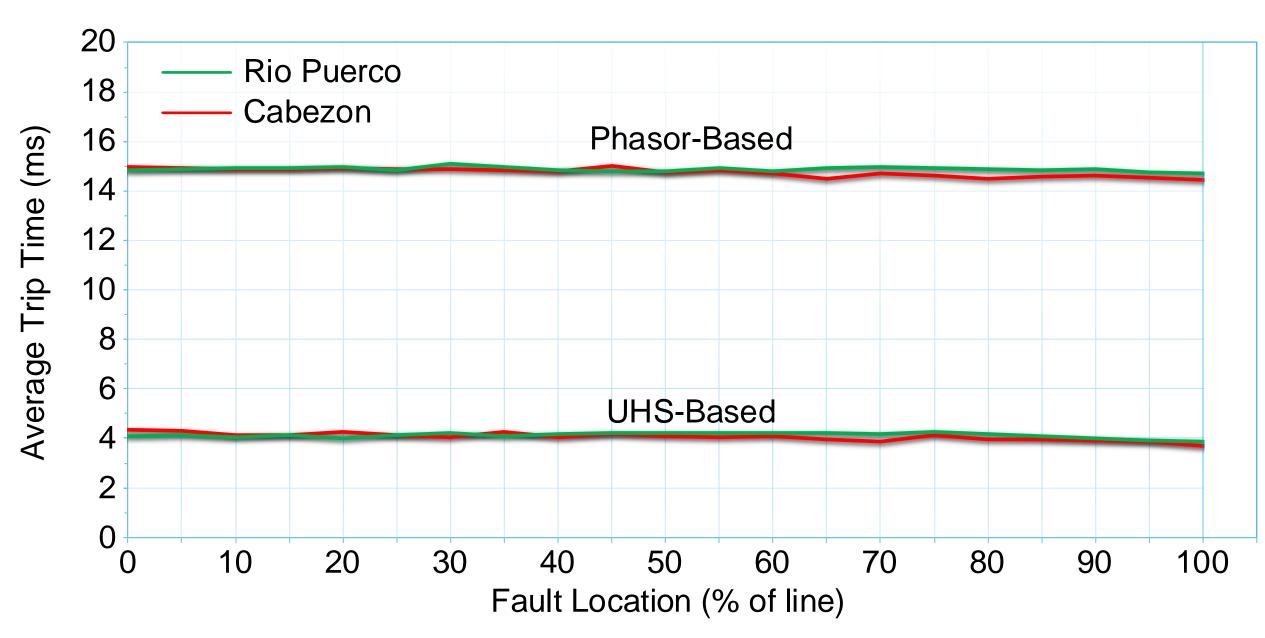
Zone 1 Performance Phasor-Based Protection



Zone 1 Performance Time-Domain Protection



Operating Time Results



How Did We Test Traveling-Wave Functions?

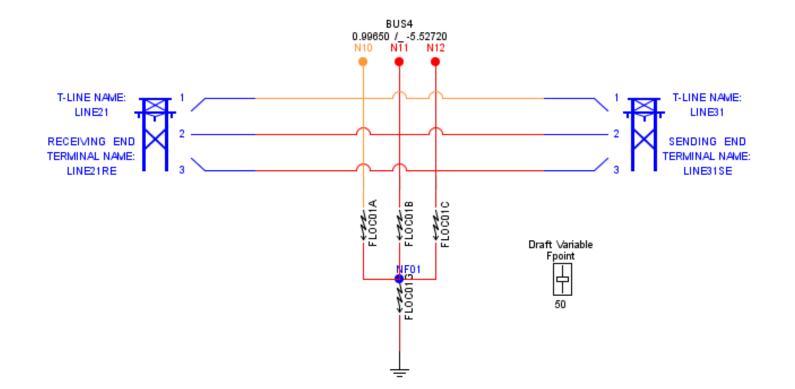


Background

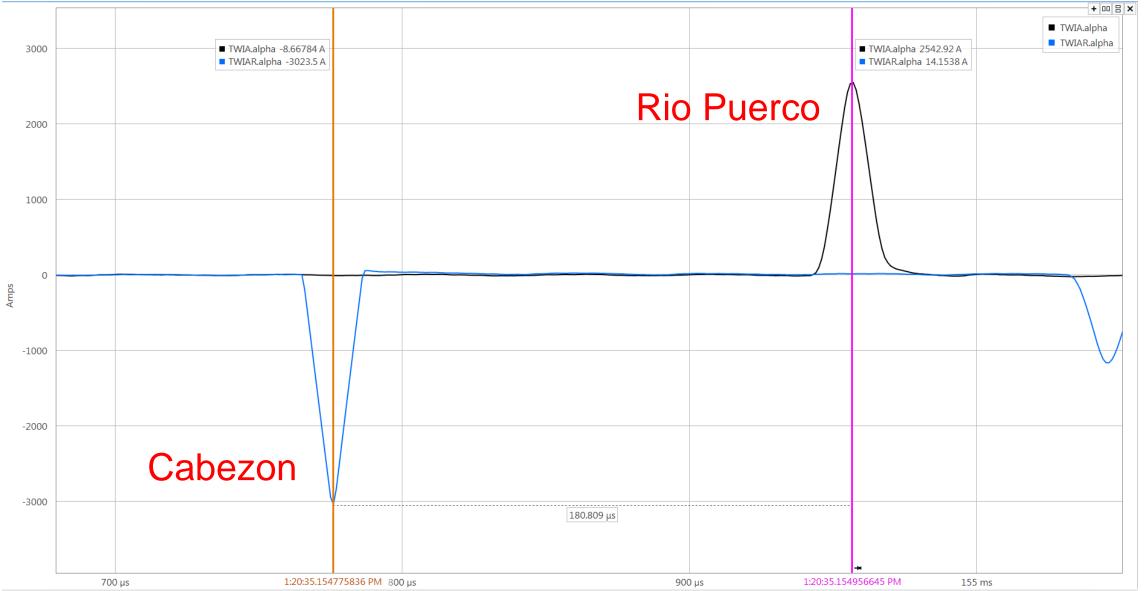
- March 2017: SEL-T400L released
- June 2017: SEL hosts Time-Domain Summit
- February 2018: RTDS demonstrates TWRT solution
- March 2018: NovaCor with TWRT arrives for evaluation
- March 2018: Customer demonstration with SEL-T400L

TWRT Test Setup

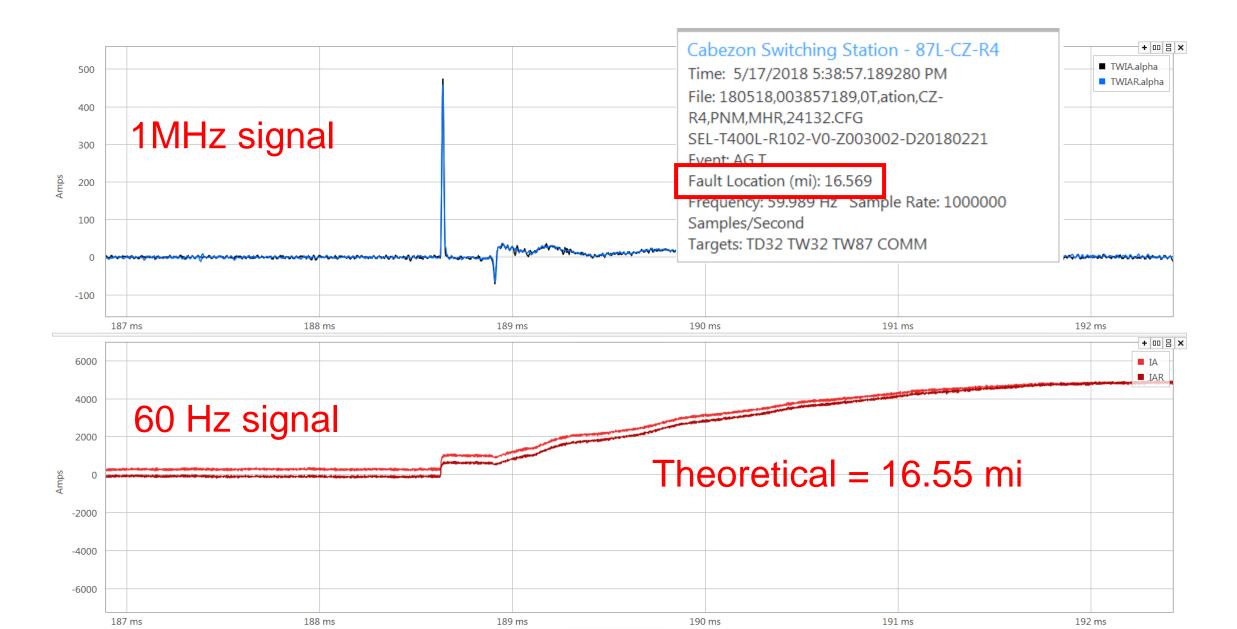
- Beta version TWRT for testing
- New GTAO firmware
- 2 microsecond time-step
- Specialized T-line models for traveling waves (TWs)
- Simple model: line under test, then a single line out from each terminal, then a source



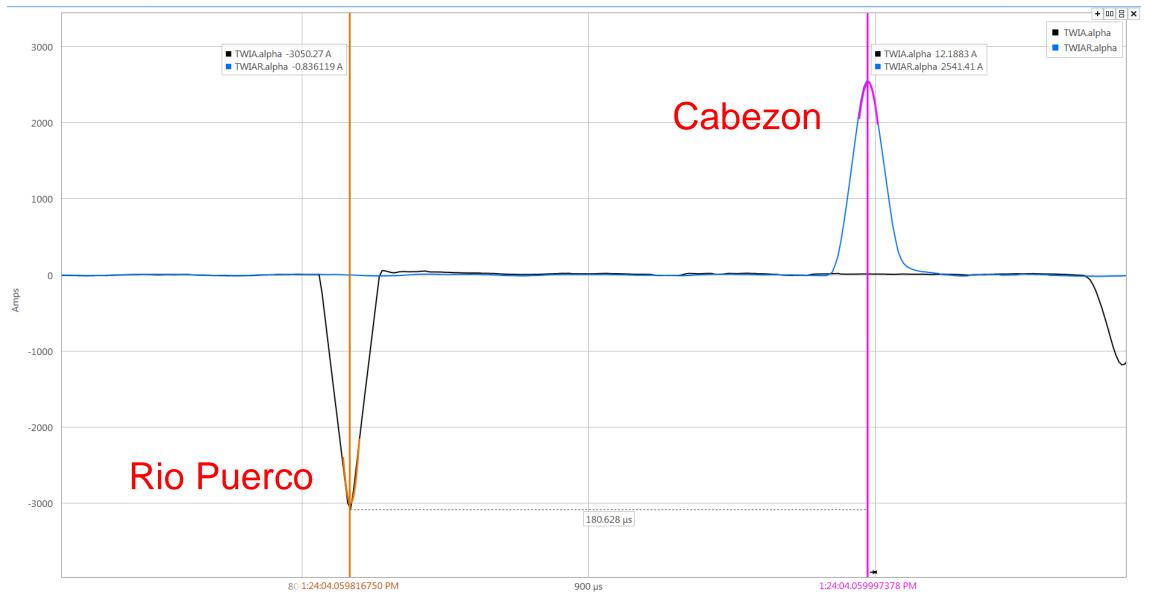
Fault Behind Cabezon Referenced From Rio Puerco



Midline Fault



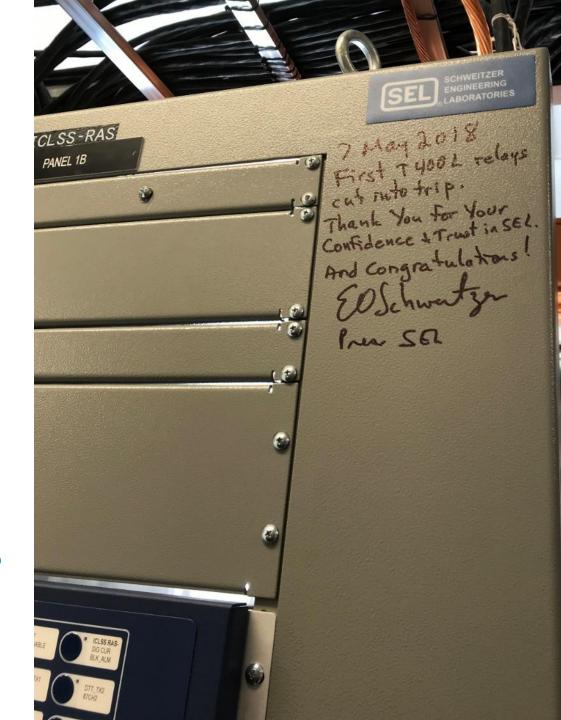
Fault Behind Rio Puerco Referenced From Rio Puerco





First Utility to Use SEL-T400L Relays for Line Protection!

May 7, 2018 Trip Outputs Connected to Breakers



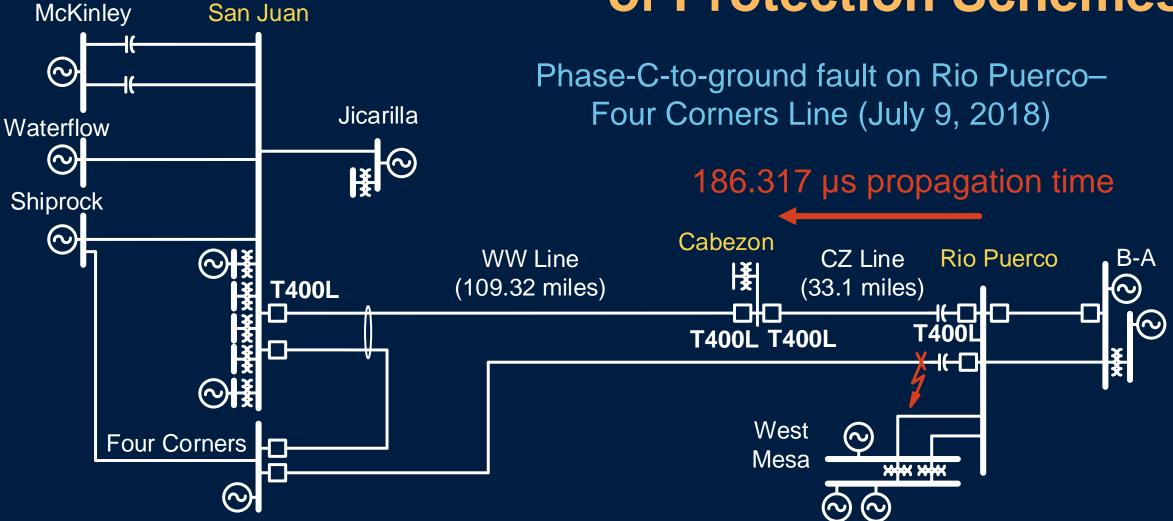


BREAKING: First ever HV transmission line protected with traveling wave relay tested by SEL on the RTDS Simulator

New Superstep tool allows users to simulate larger networks with less hardware

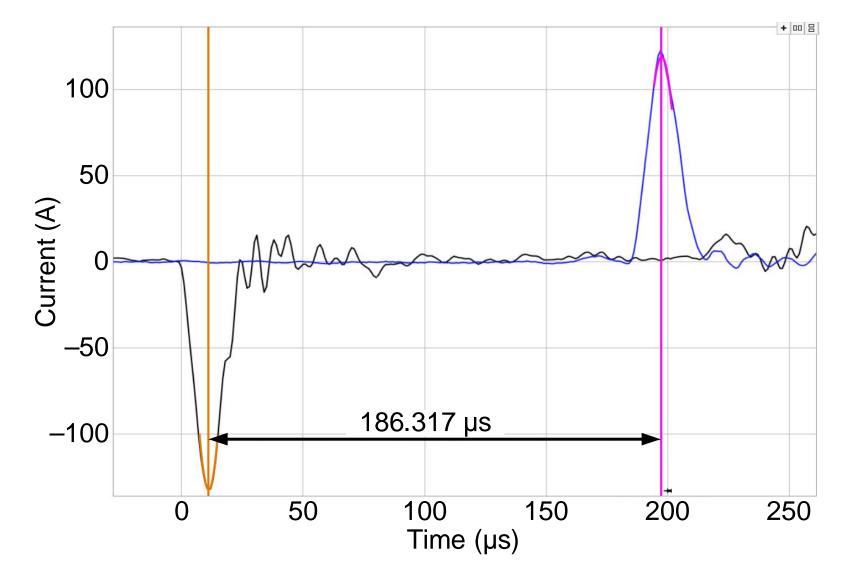
External Fault Validates Security of Protection Schemes

External Fault Validates Security of Protection Schemes



SEL-T400L Relays installed on San Juan–Cabezon and Cabezon–Rio Puerco lines

TW87 Restrains for External Fault Local and Remote TWs



PNM Has Confidence to Trip With SEL-T400L



Questions?

