



Development and Implementation of Test Systems for Protection Schemes using the RTDS Simulator

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Imagination at work

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Simulink – RTDS Conversion

System Configuration & Reconfiguration to
Test Multi-Ended Current Differential
Protection

Series Compensation in the UK

Testing an AMU in a System-Wide Context

Q&A



About Ourselves

UK Grid Solutions is a leading manufacturer of protection and control equipment with a world-wide customer base. The Grid Solutions site in Stafford UK installed their first RTDS equipment in 1997 and its primary purpose is to test protective relays and systems for validation of products under development or for customer approvals. Since 2011 the laboratory has been accredited by UKAS to IEC17025.



Simulink – RTDS Conversion

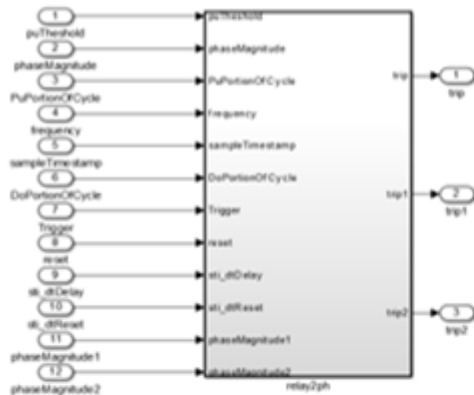


Introduction on Simulink – RTDS Conversion

- RTDS technologies provide an interface between Matlab Simulink models and RSCAD.
- The approach is to make use of the C code generator in Matlab Simulink to generate code in a form suitable for RSCAD C Builder. Import the generated code into C Builder and create the RSCAD component
- Benefits of making use of the conversion: make it possible to test algorithms in real time before hardware is available; the converted model could be imported as a component into existing power system protection RTDS test cases.



Conversion Study(1/2)



Simulink model

Code Generation



```
// Include file below is generated by C-Builder
// and contains the variables declared as -
// PARAMETERS, INPUTS, OUTPUTS . . .
#include "NewSampler.h"

STATIC:
// We want to sample one time over Cat.
double Cat ;
int opt ;
double dt ;

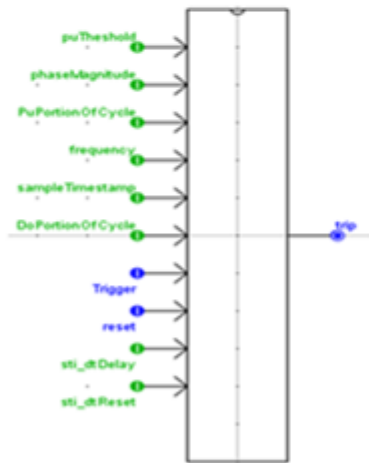
SAM_FUNCTIONS:
SAM:
dt = getTimeStep() ;

CODE:
Cat = 1/ (Freq * Num * dt) ;

if ( opt > Cat-1 ) {
    opt = 1 ;
    Trigg = 1 ;
}
else{
    opt++ ;
    Trigg = 0 ;
}
}
```

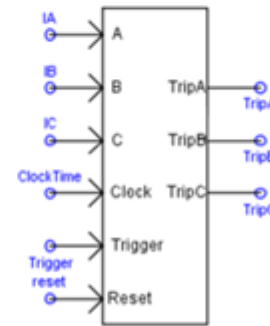
C codes

Import Simulink Model



RTDS component

Change inputs into settings



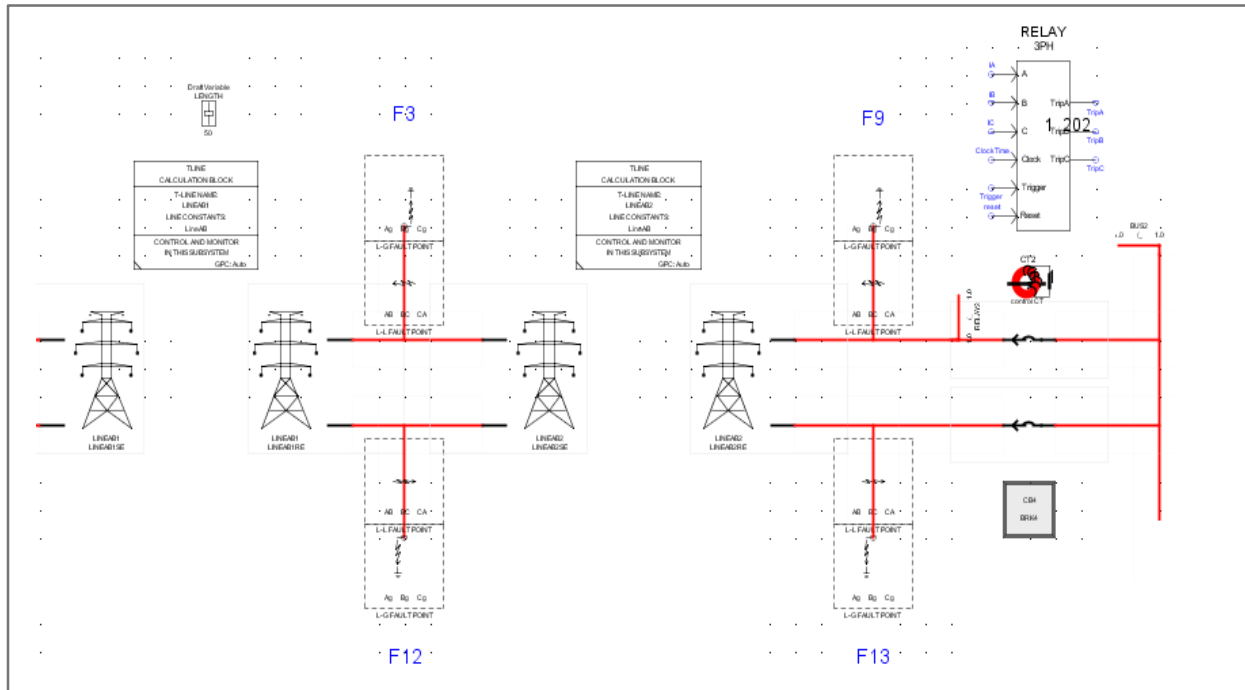
Simplified RTDS component

Put component into draft

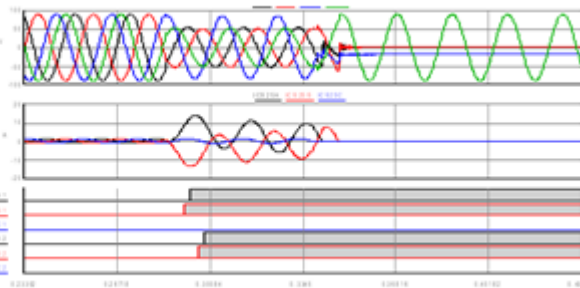


Conversion Study (2/2)

(Put component into draft)



Run the Simulation

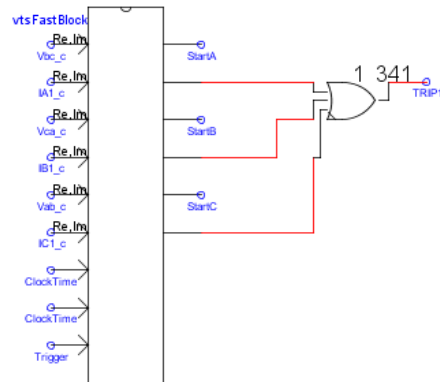
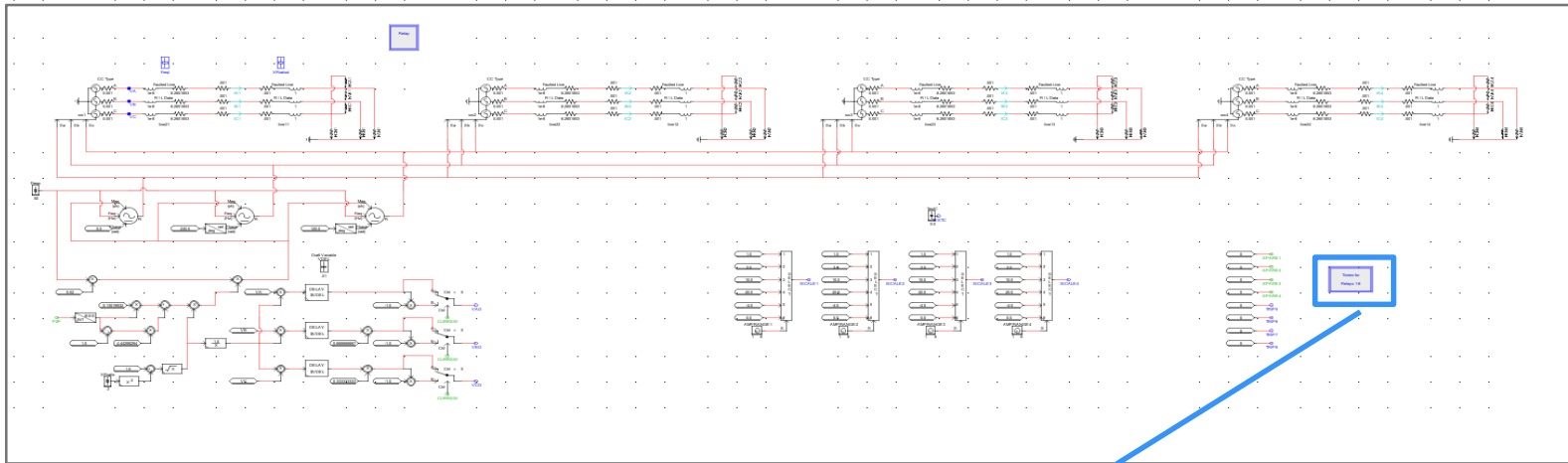


RTDS Simulation result



Case Study

- CT requirement testing system under RTDS environment



the Converted component in testing system

- Same tests were performed on the converted model and on a real overcurrent relay. The results are very close.

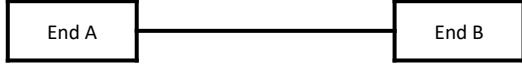


System Configuration & Reconfiguration to Test Multi-Ended Current Differential Protection

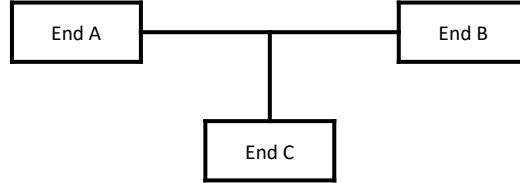


System Configurations to Test (1/2)

2 Ended

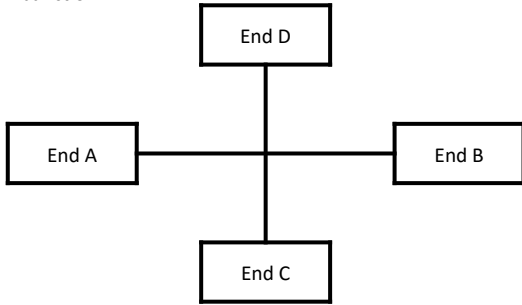


3 Ended

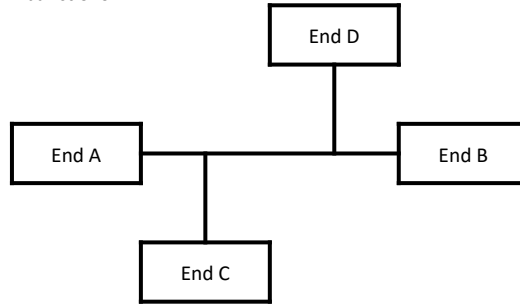


4 Ended

1 Junction

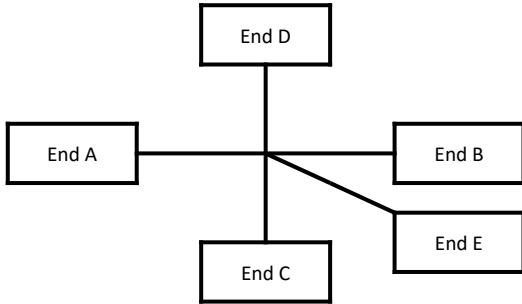


2 Junctions

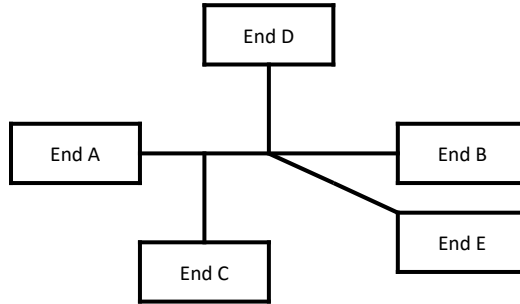


5 Ended

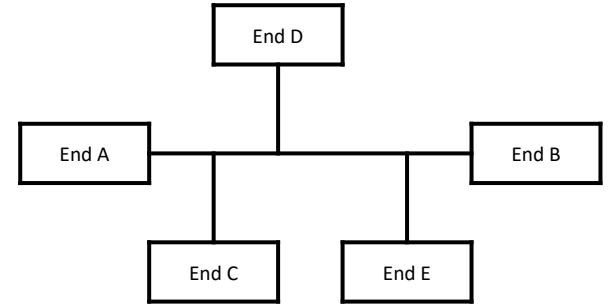
1 Junction



2 Junctions



3 Junctions



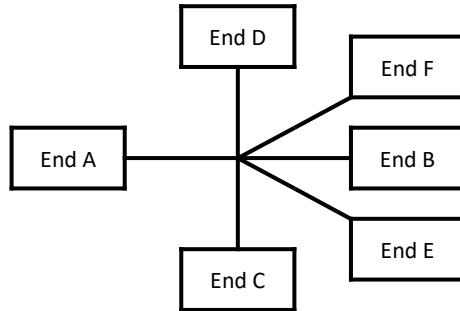
- There are 13 configurations in total to cover for this Multi-Ended current differential protection validation testing.



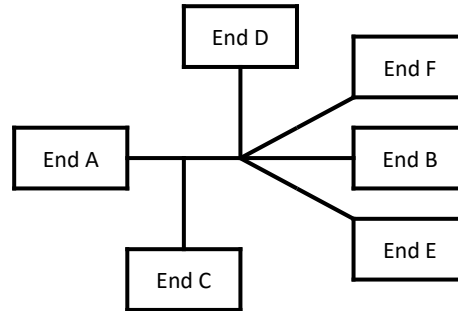
System Configurations to Test (2/2)

6 Ended

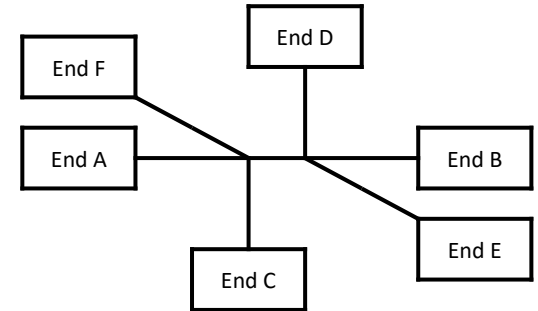
1 Junction



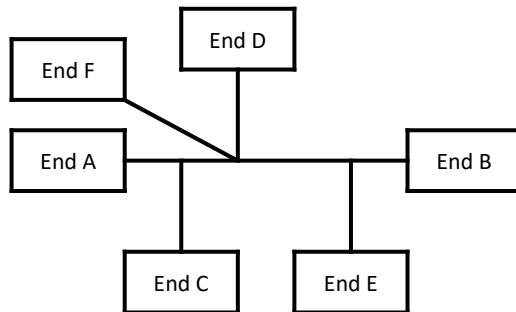
2 Junctions (alt 1)



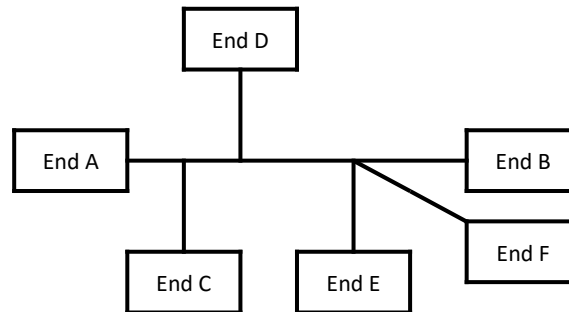
2 Junctions (alt 2)



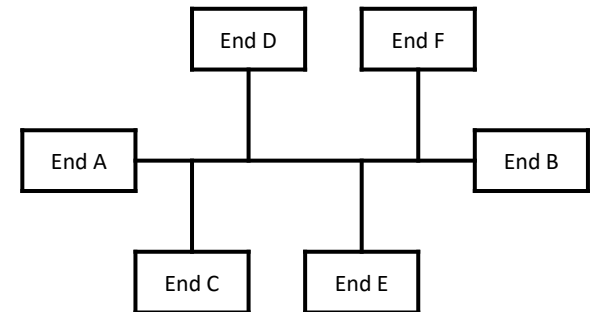
3 Junctions (alt 1)



3 Junctions (alt 2)

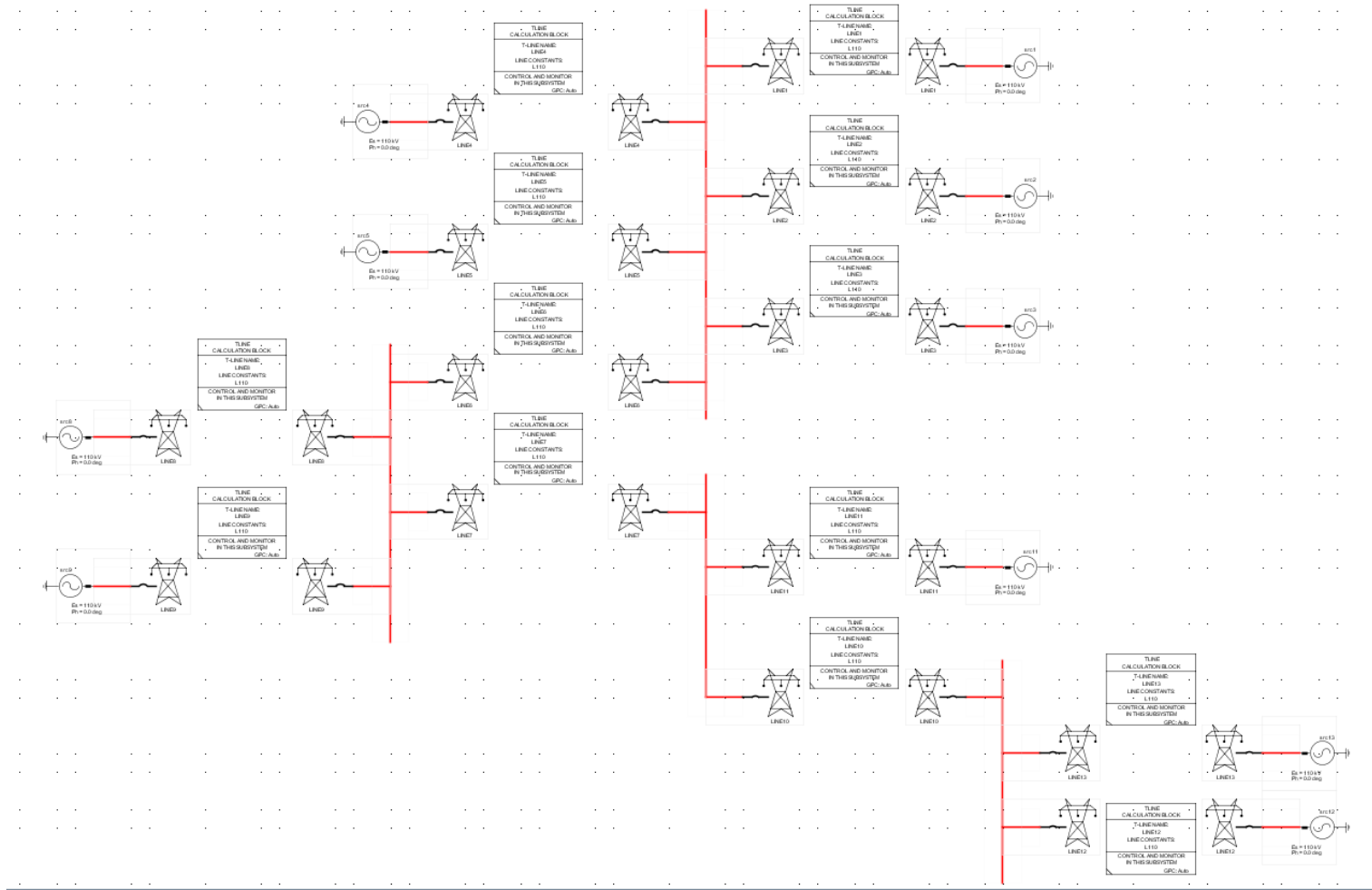


4 Junctions

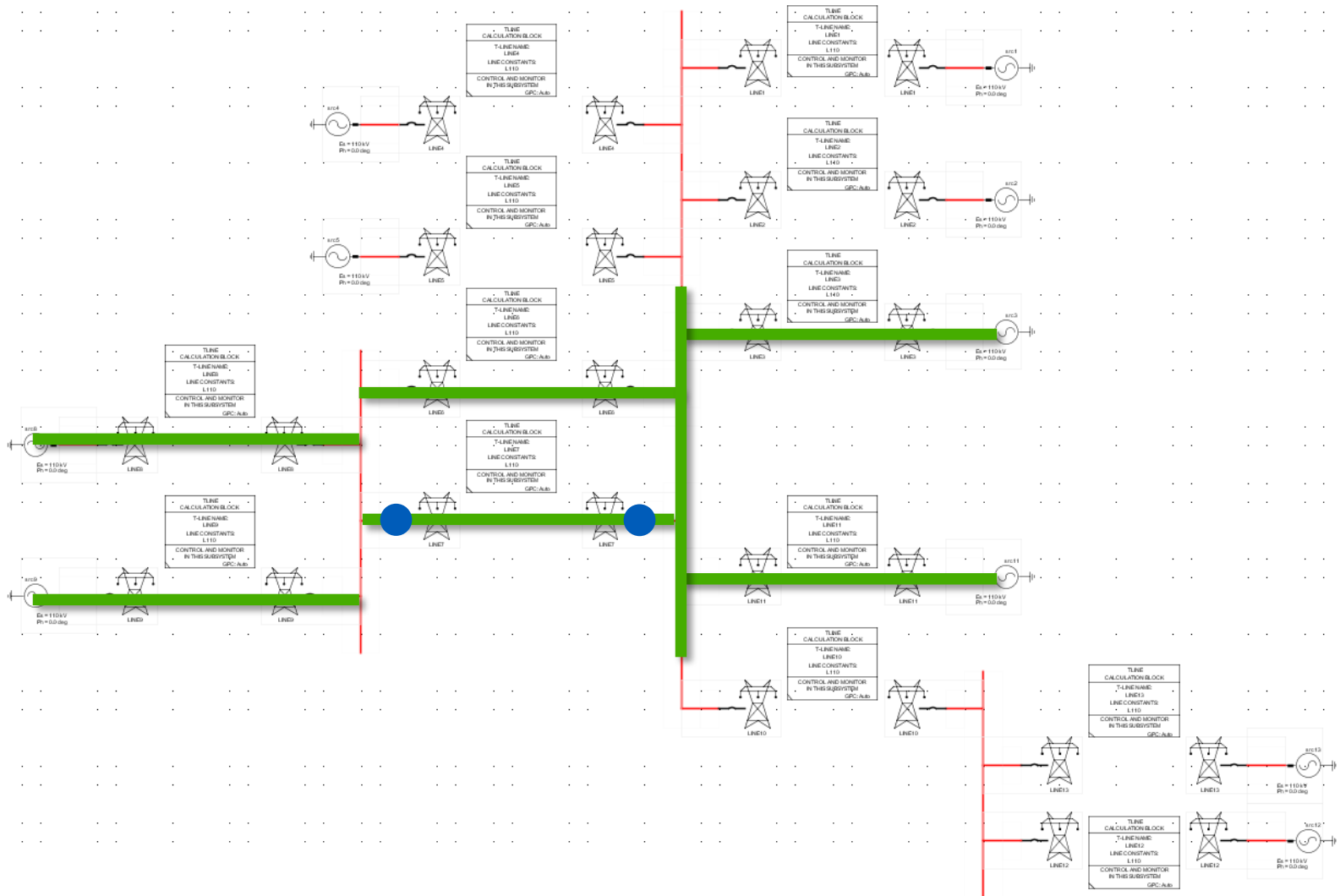


Overall System Configuration

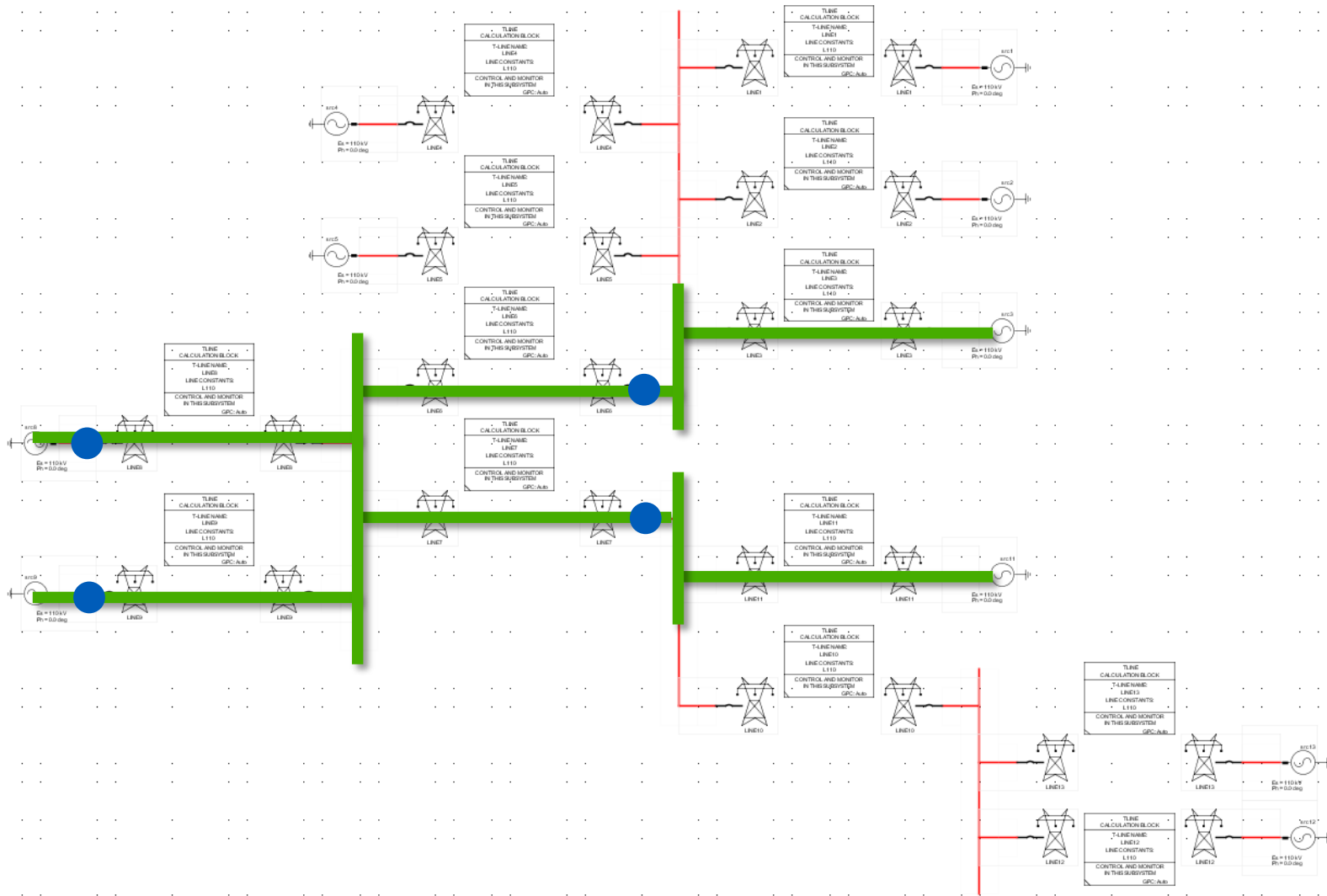
- We implemented 1 single system to cover all of them



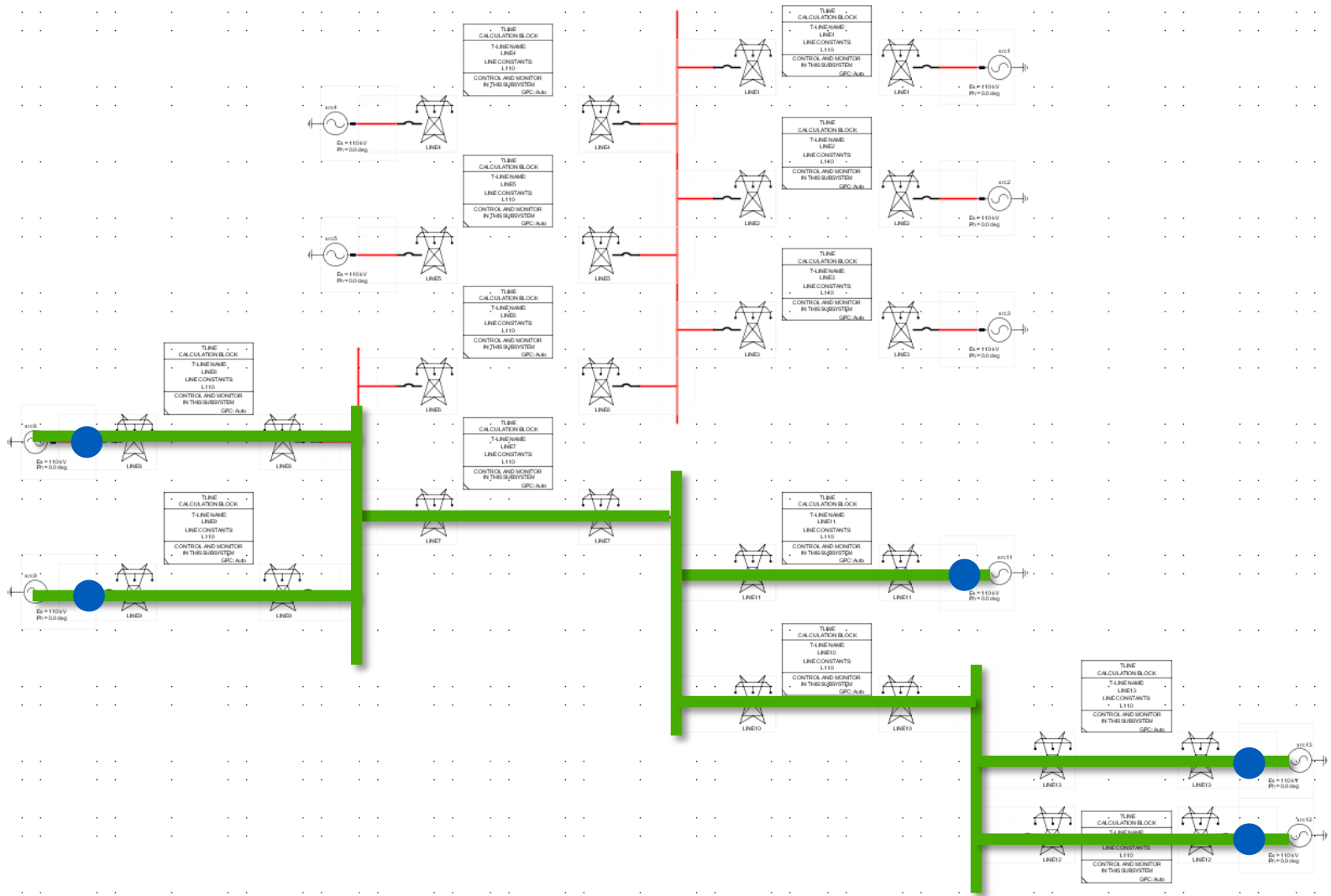
Test Configuration(1/4) – 2 Terminals



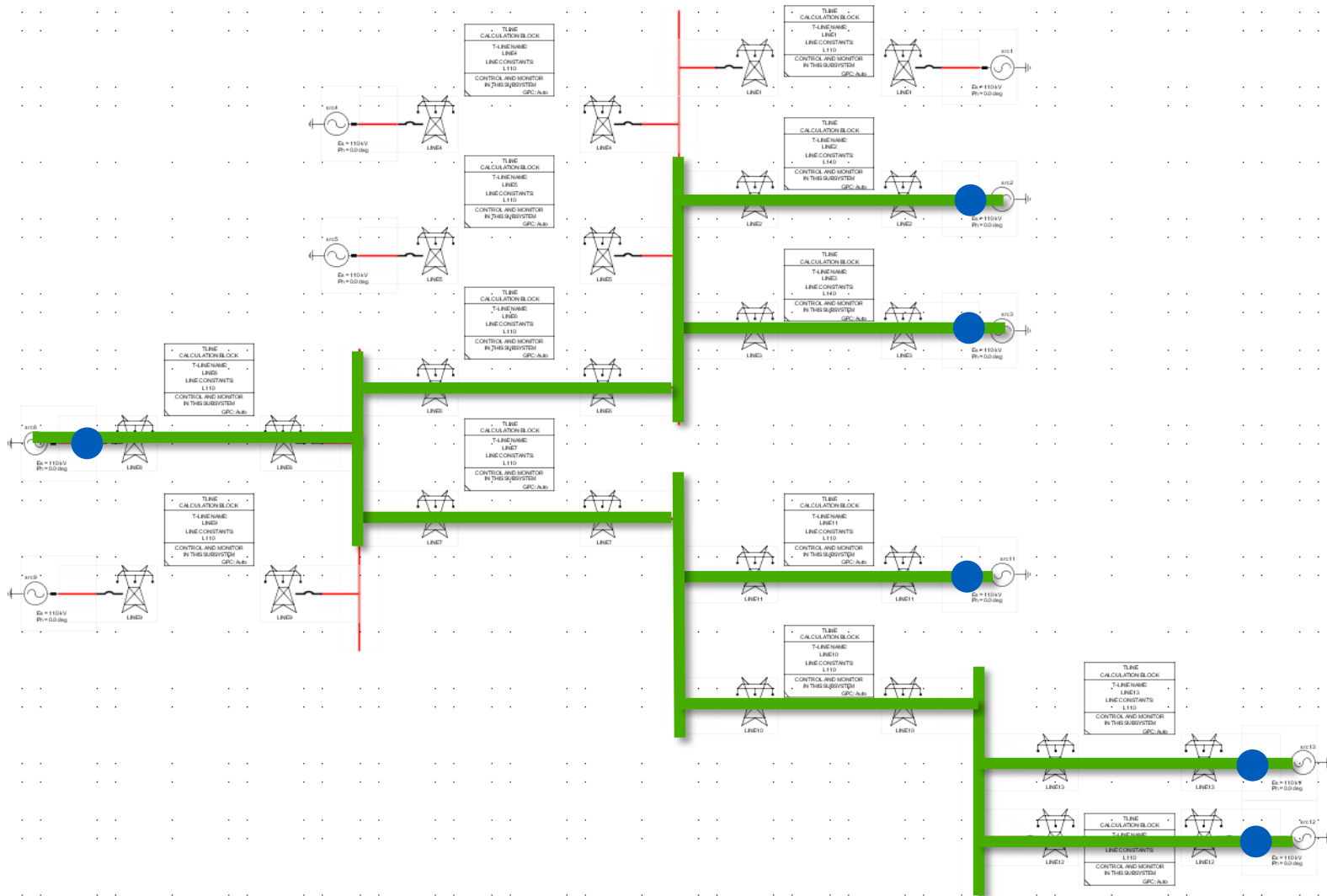
Test Configuration(2/4) – 4 Terminals 1 Junction



Test Configuration(3/4) – 5 Terminals 3 Junctions



Test Configuration(4/4) – 6 Terminals 4 Junctions



Series Compensation in the United Kingdom



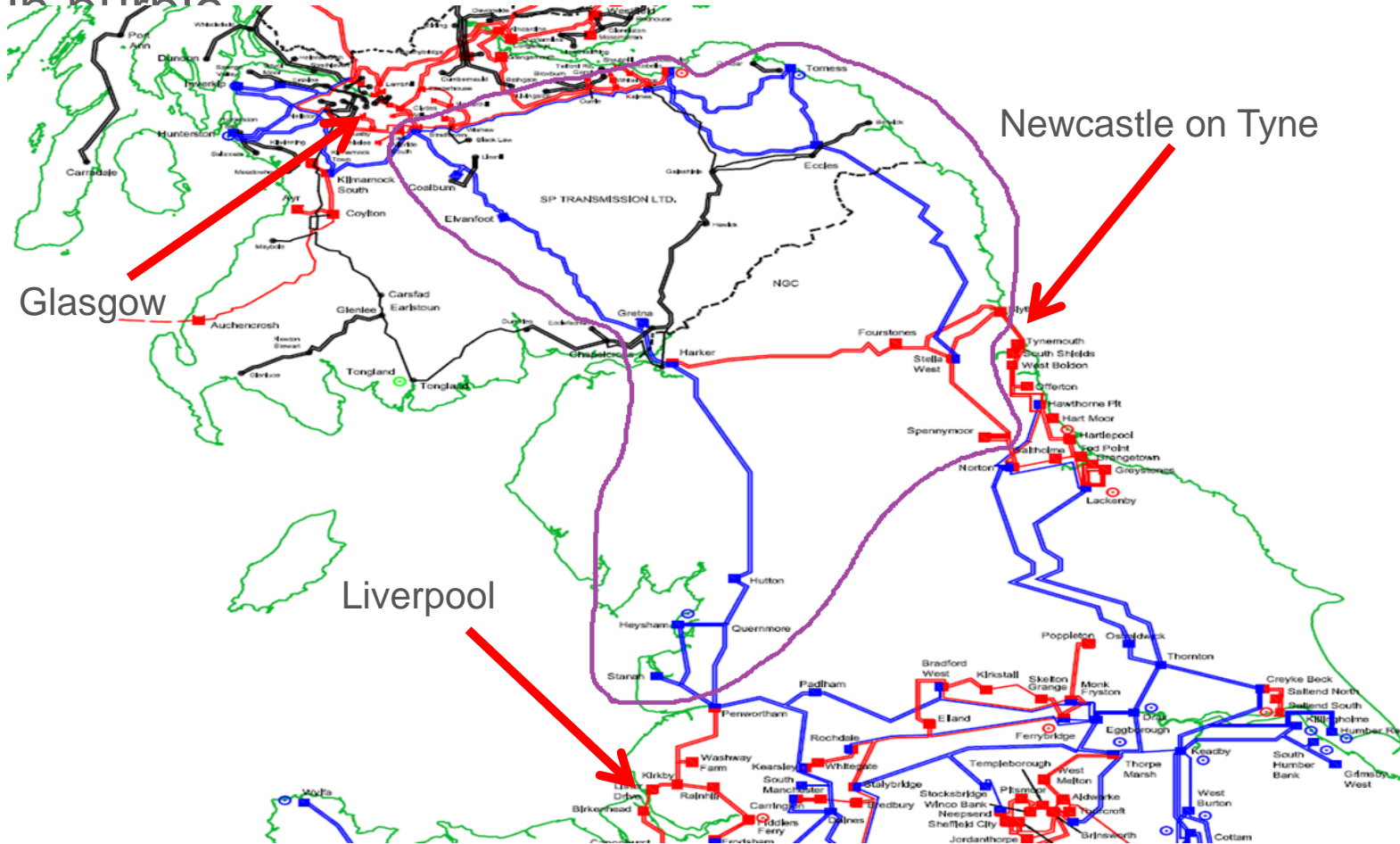
Background

- Changing locations of power generation in the United Kingdom are demanding additional capacity to transfer power from Scotland to England.
- New line construction considered too expensive.
- Utilising series compensation to improve system stability; thus allowing the existing lines to be operated closer to their thermal capacity.
- Dense and interconnected network raises questions over the impact on existing protection on the adjacent lines.
- Important connections close to capacitors; e.g. nuclear generation, feed for major railway.



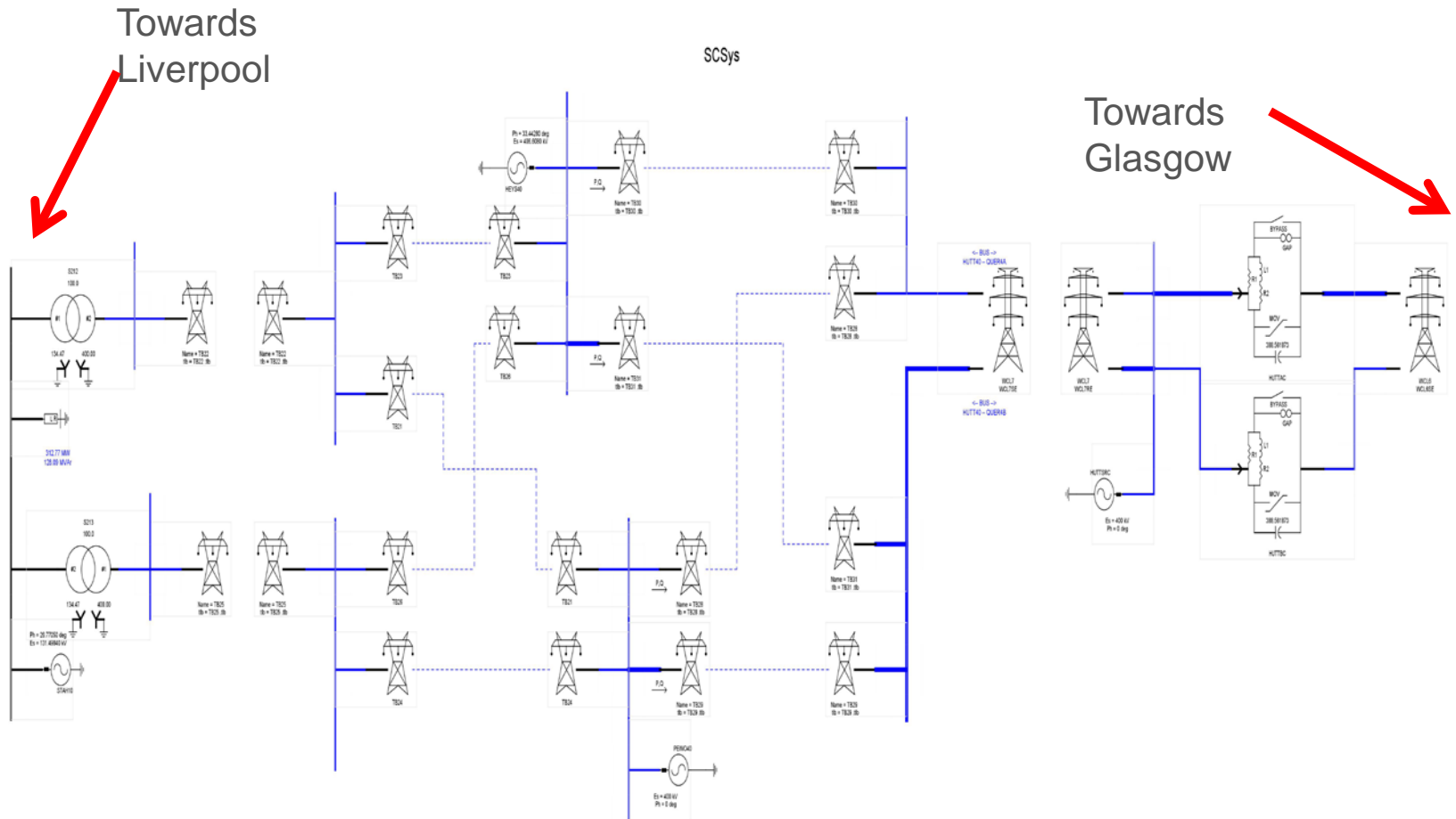
Area covered by Study

- All the 400kV lines (in blue); 275kV lines (in red) and some of the 132 KV lines (in black) in the area enclosed in purple



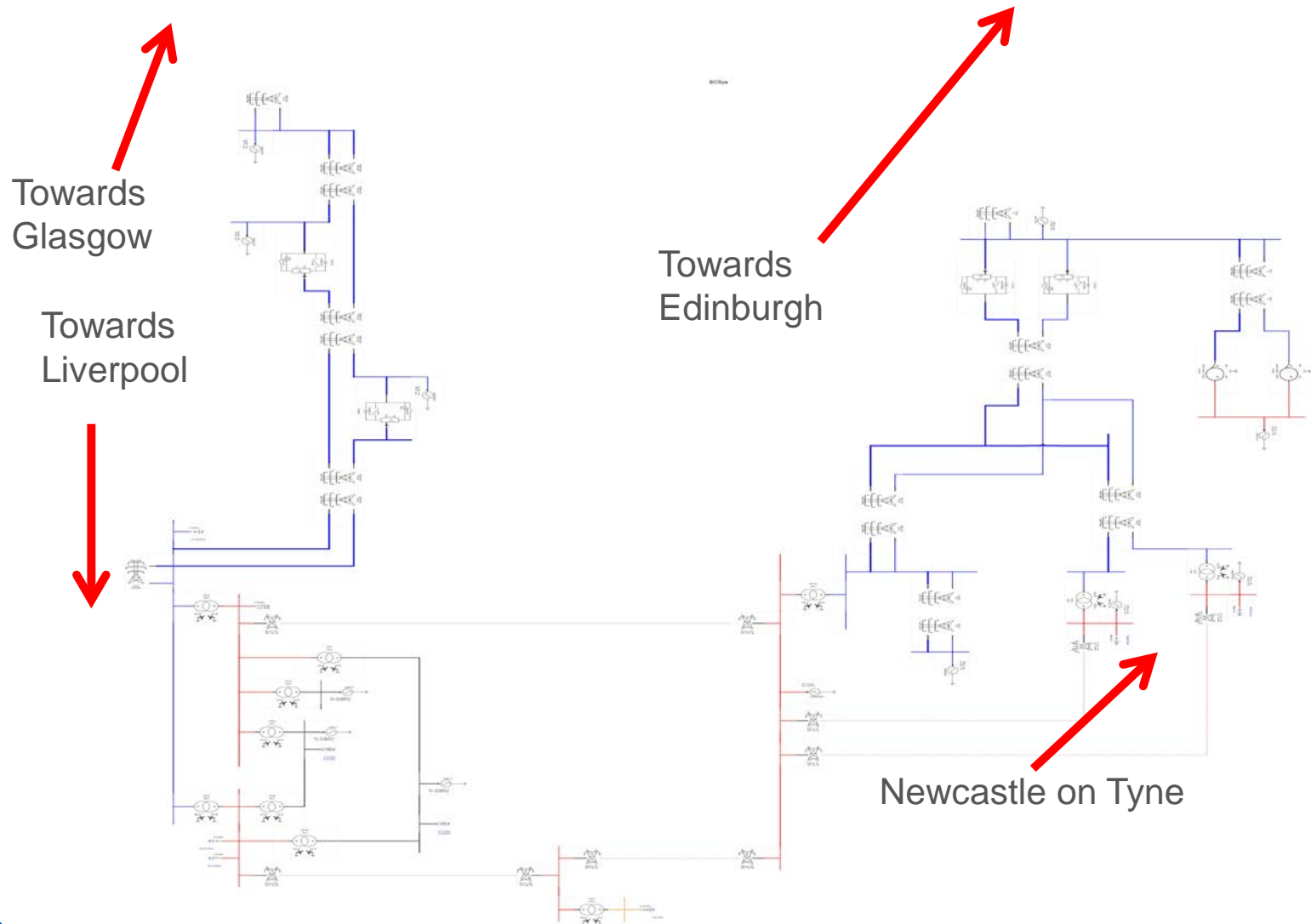
RTDS Case – South Western part

- Thick Lines show which lines were tested



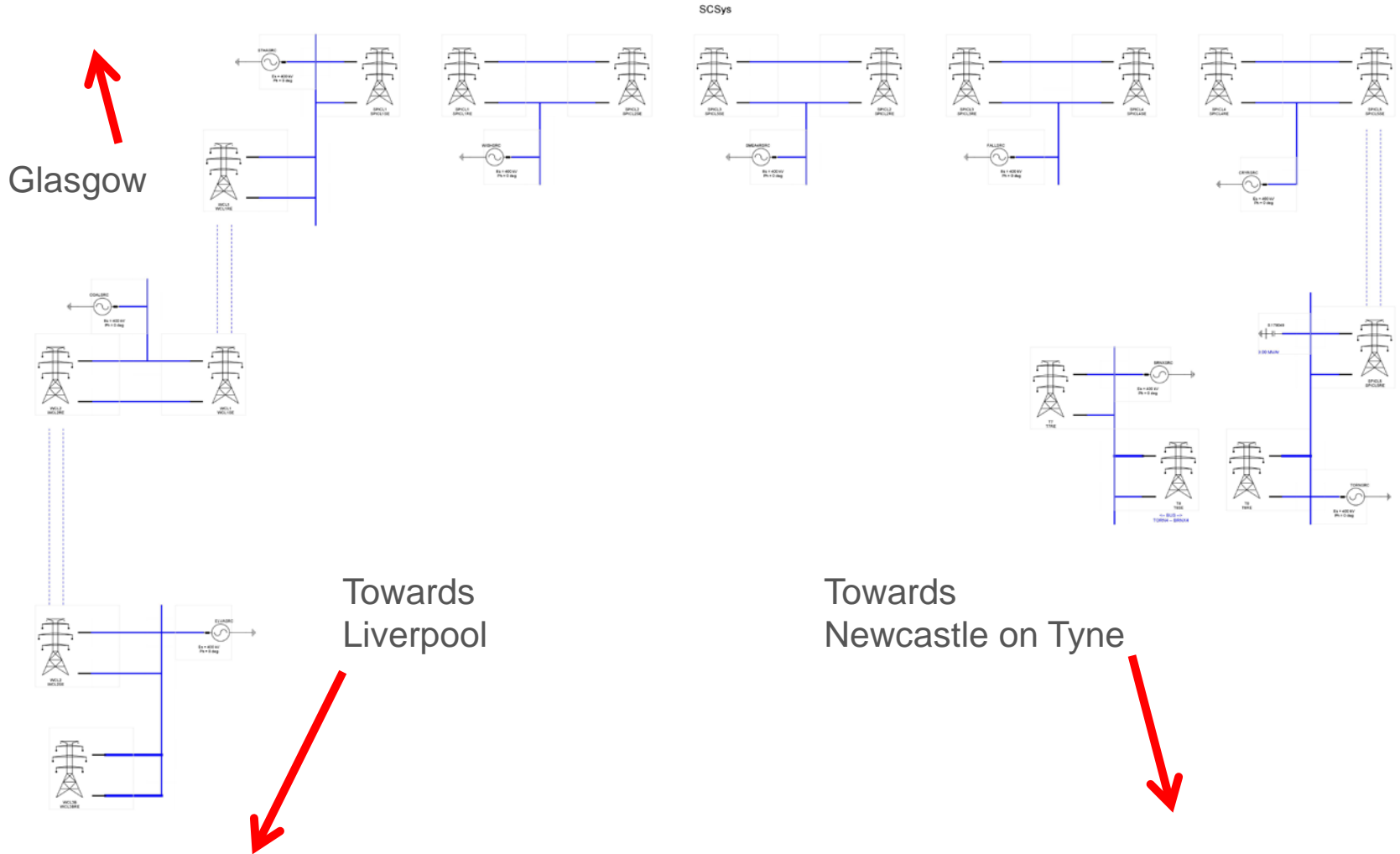
RTDS Case – Central part

- Thick Lines show which lines were tested



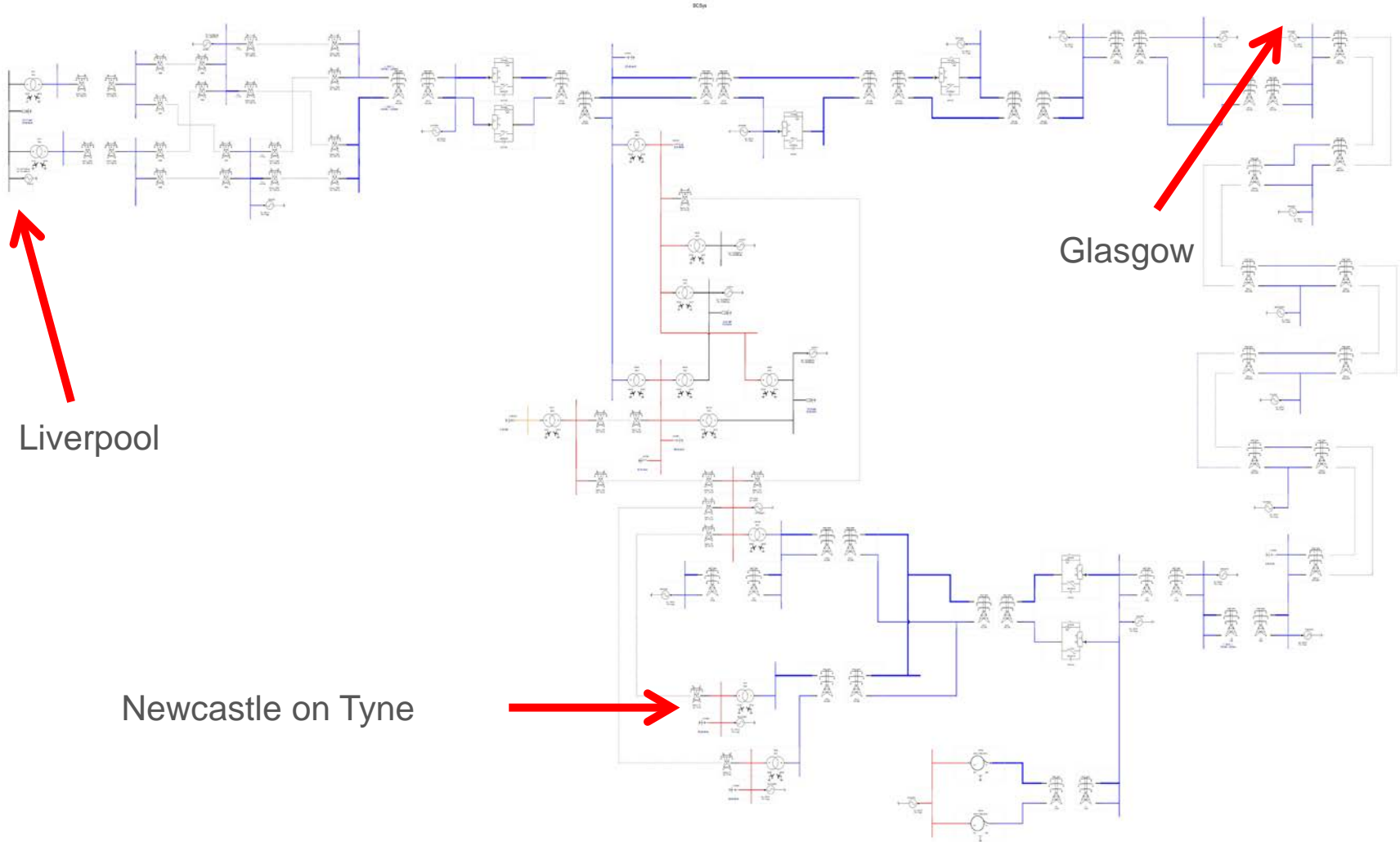
RTDS Case – Northern part

- Thick Lines show which lines were tested



RTDS Case

- Thick Lines show which lines were tested



Testing an AMU in a System-Wide Context

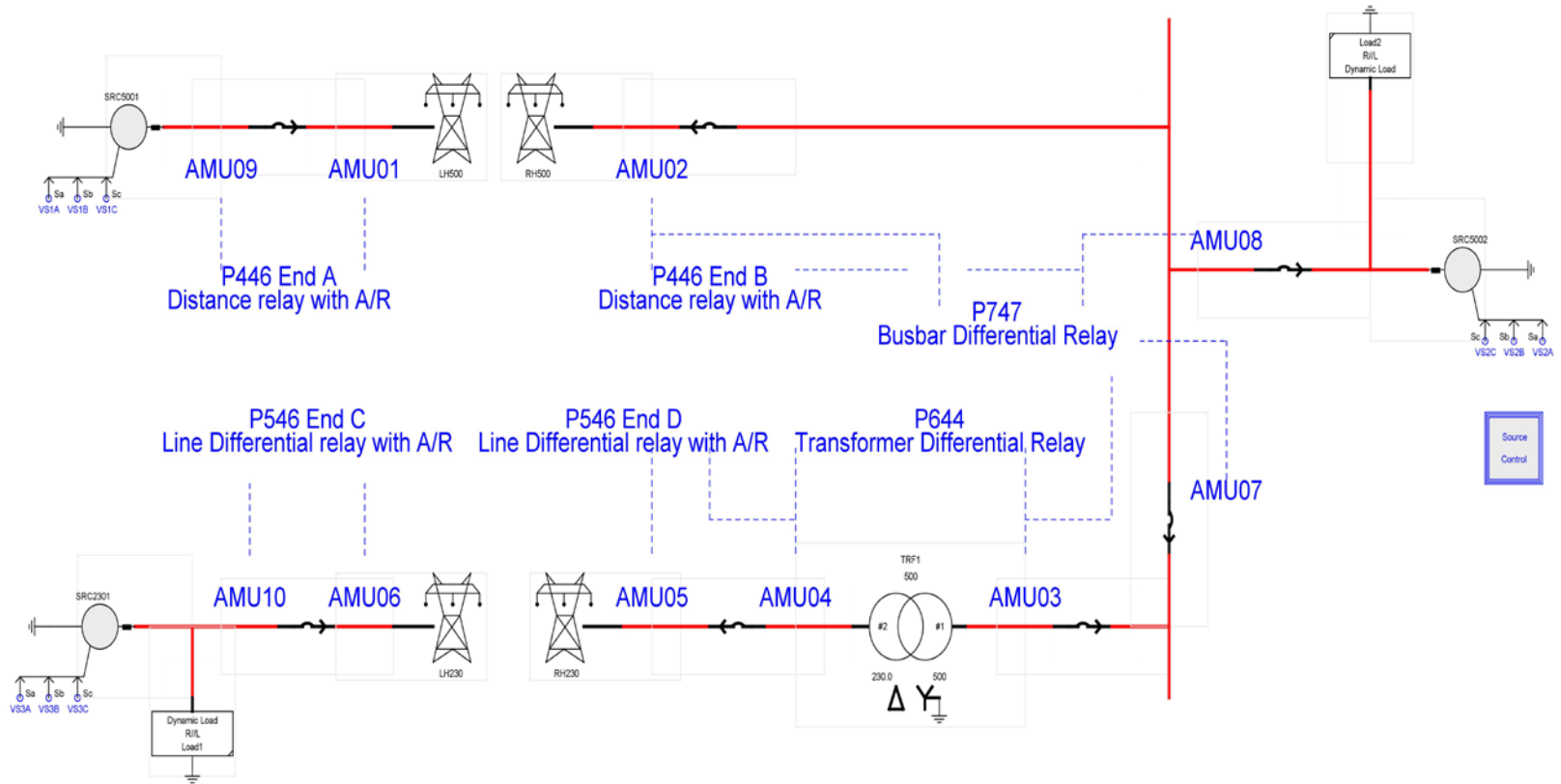


Test requirements

- Part of validation of an AMU design before product launch.
- Need to examine performance when used as a complete system.
 - Multiple AMU devices
 - Various protective relays
- Representative of the lead customer's system (500kV).



RTDS Case



Characteristics of Test System

- Internal faults for one protection are external faults for the others.
 - Reduces overall number of tests
- Complex system to configure.
 - Needs large numbers of amplifiers
 - Space required for relays and network equipment
- Requires synchronisation.
- All ten AMU outputs merged into one datastream sent to all relays.
- Measured operating times to be compared with those expected of conventional protection.





Q&A

Thank you !



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Appendix- Case Study of Simulink – RTDS Conversion

- Same tests were performed on the converted model and also on a real overcurrent relay. Figures below display tripping time in seconds for internal phase-to-ground fault for a fixed CT knee-point voltage and CT secondary lead burden varying from 0.1 ohm to 13 ohms. Tripping time in green is fast operation and yellow reflects normal operation

	Ftyp	XR	In	If	Shot	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1	1.2
Real relay	PGF	120	1	10	1	0.3427	0.3681	0.3831	0.4024	0.4324	0.4447	0.4632	0.4902	0.4923	0.5168	0.5373
	PGF	120	1	10	2	0.3616	0.3867	0.4028	0.4230	0.4420	0.4649	0.4845	0.5010	0.5114	0.5269	0.5484
	PGF	120	1	10	3	0.3622	0.3870	0.4042	0.4230	0.4422	0.4648	0.4834	0.5010	0.5126	0.5280	0.5473
	PGF	120	1	10	4	0.3218	0.3470	0.3631	0.3840	0.4025	0.4254	0.4440	0.4711	0.4724	0.4977	0.5282
	PGF	120	1	10	5	0.3632	0.3876	0.4030	0.4236	0.4432	0.4641	0.4835	0.5005	0.5120	0.5270	0.5481
	PGF	120	1	10	6	0.3625	0.3868	0.4038	0.4237	0.4441	0.4643	0.4835	0.5007	0.5121	0.5284	0.5489
scientific model	PGF	120	1	10	1	0.3395	0.3595	0.3796	0.3995	0.4196	0.4396	0.4496	0.4696	0.4895	0.4996	0.5296
	PGF	120	1	10	2	0.3496	0.3695	0.3995	0.4196	0.4396	0.4595	0.4796	0.4895	0.5095	0.5196	0.5396
	PGF	120	1	10	3	0.3496	0.3695	0.3995	0.4196	0.4396	0.4595	0.4796	0.4895	0.5095	0.5196	0.5396
	PGF	120	1	10	4	0.3196	0.3395	0.3595	0.3796	0.3995	0.4096	0.4396	0.4496	0.4696	0.4796	0.5095
	PGF	120	1	10	5	0.3496	0.3695	0.3995	0.4196	0.4396	0.4595	0.4796	0.4895	0.5095	0.5196	0.5396
	PGF	120	1	10	6	0.3496	0.3695	0.3995	0.4196	0.4396	0.4595	0.4796	0.4895	0.5095	0.5196	0.5396



Appendix- Case Study of Simulink – RTDS Conversion

	Ftyp	XR	In	If	Shot	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1	1.2
Real relay	PGF	120	1	20	1	0.2121	0.2318	0.2667	0.2833	0.3182	0.3267	0.3327	0.3476	0.3565	0.3676	0.3897
	PGF	120	1	20	2	0.2330	0.2631	0.2861	0.3030	0.3279	0.3364	0.3537	0.3675	0.3775	0.3870	0.3995
	PGF	120	1	20	3	0.2338	0.2620	0.2862	0.3033	0.3275	0.3368	0.3532	0.3676	0.3763	0.3870	0.3984
	PGF	120	1	20	4	0.1833	0.2127	0.2369	0.2639	0.2977	0.2970	0.3128	0.3381	0.3473	0.3671	0.3884
	PGF	120	1	20	5	0.2329	0.2634	0.2862	0.3028	0.3283	0.3366	0.3525	0.3676	0.3776	0.3866	0.3990
	PGF	120	1	20	6	0.2336	0.2623	0.2863	0.3039	0.3293	0.3358	0.3537	0.3676	0.3767	0.3865	0.3991
scientific model	PGF	120	1	20	1	0.1996	0.2296	0.2495	0.2795	0.2995	0.3095	0.3196	0.3395	0.3496	0.3595	0.3695
	PGF	120	1	20	2	0.2296	0.2495	0.2795	0.2995	0.3196	0.3295	0.3496	0.3595	0.3695	0.3796	0.3896
	PGF	120	1	20	3	0.2296	0.2495	0.2795	0.2995	0.3196	0.3295	0.3496	0.3595	0.3695	0.3796	0.3896
	PGF	120	1	20	4	0.1796	0.1996	0.2296	0.2495	0.2795	0.2896	0.2995	0.3196	0.3395	0.3496	0.3695
	PGF	120	1	20	5	0.2296	0.2495	0.2795	0.2995	0.3196	0.3295	0.3496	0.3595	0.3695	0.3796	0.3896
	PGF	120	1	20	6	0.2296	0.2495	0.2795	0.2995	0.3196	0.3295	0.3496	0.3595	0.3695	0.3796	0.3896

- From the results we could see that the results on the real relay and scientific model follow a similar pattern. Taking account of the noise which hasn't been included in the scientific model testing, the results are really similar. The preliminary conclusion that the conversion of this scientific model is successful can be made.

